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INTERACTIVE TIME RECURSIVE STATE ESTIMATOR PROGRAM(U)  
ARMY MISSILE COMMAND REDSTONE ARSENAL AL GUIDANCE AND  
CONTROL DIRECTORATE S BRAZELTON MAY 85

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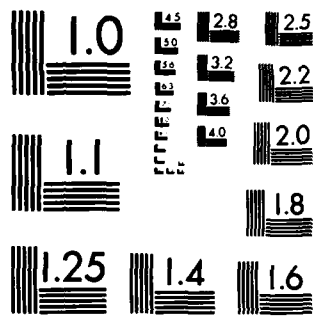
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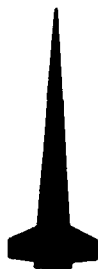
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TECHNICAL REPORT RG-85-20

INTERACTIVE TIME RECURSIVE STATE  
ESTIMATOR PROGRAM

Sandra Brazelton  
Guidance and Control Directorate  
US Army Missile Laboratory

May 1985

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The SHORAD C <sup>2</sup> system consists of the equipment necessary to provide command and control capability for Army divisional and non-divisional Air Defense Artillery (ADA). This report describes a technique for smoothing noisy track data using a GHK discrete time-recursive state estimator program. This computer program was developed as part of an analysis of SHORAD track management functions. This system will show how accurately a target can be tracked given the appropriate input values.		

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## I. INTRODUCTION

The Short Range Air Defense Command and Control (SHORAD C<sup>2</sup>) system consists of the equipment necessary to provide C<sup>2</sup> capability for Army divisional and non-divisional Air Defense Artillery (ADA). It will provide C<sup>2</sup> for all echelons of a SHORAD battalion. The network will consist of displays, data processors, interface equipment, and sensors. The major objectives of the system are:

- Provide automated alert to all SHORAD battalion elements.
- Provide for automatic exchange of command information between SHORAD battalion elements.
- Provide weapon cueing to selected SHORAD battalion elements.
- Provide track information from the various sensor inputs to SHORAD C<sup>2</sup>. This involves track management functions which include track file management and track smoothing operations.

Track files from external sensors such as PATRIOT, TSQ-73, HAWK, ADEWS, and AWACS feed data into high level modes of SHORAD C<sup>2</sup>. Track management functions include the maintenance, correlation, triangulation and smoothing of track data. This report describes a technique for smoothing noisy track data using a GHK discrete time-recursive state estimator program. The GHK estimator is useful in smoothing noisy track data obtained from noisy measurement sensors in applications such as the C<sup>2</sup> system for SHORAD. This computer program was developed as part of an analysis of SHORAD track management functions.

A detailed description of inputs and calculations will be included in the discussion to assist the user in choosing the original values. In addition, examples of inputs, resulting calculations, and plots will be provided in the results to give the user a thorough understanding of the output. Also, the necessary system assignment statements to aid the user in obtaining a hard copy of the results will be included in Appendixes A - C.

## II. DISCUSSION

Initial values are input to determine the initial position, velocity, and acceleration of the target. The program then estimates the current position, velocity, and acceleration at each discrete time, based on initial conditions and a predefined predictor/estimator logic. Noise and various maneuvers may be added to the true position to determine how accurately the estimator handles noisy sensor data on maneuvering targets. Plots of true and estimated positions may be obtained to analyze the adequacy of filtering logic.

NOTE: Name of output entered is used as graph title.

### A. Inputs

#### 1. Main Program Inputs

<u>VARIABLE</u>	<u>FORMAT</u>	<u>DESCRIPTION</u>
-----------------	---------------	--------------------

SEED	15	Used to generate random numbers. Must be an odd integer $0 < \text{SEED} < 32768$ . The SEED is used to generate a unique set of random numbers.
------	----	--

XBAR	F6.2	Estimate of position.
XDBAR	E12.5	Time derivative estimate.
XDDBAR	E12.5	Estimate of acceleration.
B	E16.9	BETA - BETA may be entered from the keyboard or computed. Please refer to calculation section for computation.
G,H,K	E12.5	NOTE - G, H, and K are a function of BETA. Please refer to calculation section for computations.
SIG	F6.2	Noise SIGMA.
MEAN	F6.2	Noise MEAN.
Z1	E12.5	Initial true position.
XD1	E12.5	Initial time derivative.
TIME	F6.2	Initial time.
DELT	F6.2	Time increment.
TM	F6.2	Time of maneuver start.
IMAX	I3	Number of computation steps.

All inputs except IMAX and SEED are floating point.

NOTE: An option is available so that if one chooses to rerun the program, he will not have to reenter the original values. When this option is chosen, the user can change only the specific value(s) of interest to him.

## 2. Inputs for Subroutine BETA

TC	F5.2	Time constant
DELT	F5.2	Time increment

## B. Computations

### 1. Subroutine BETA-BETA is computed as follows:

$E = 2.718281828$   
 $LAM = 1./TC$   
 $X = LAM \times DELT$

$BETA (B) = E^{**X}$

so BETA = .967216134.



## 2. Subroutine GHK

$G = 1. - B^{**3}$   
 $H = 3./2. \times ((1. - B^{**2}) \times (1. - Y)); (Y = \text{noisy position measurement})$   
 $K = 1./2. \times ((1. - Y) **3)$

## 3. Main Program

### a. Target Computation

Target acceleration is computed as follows:

$ZDD = 78.5 (T - TM)$   
IF (ZDD.GE.49.1) then ZDD = 49.1

User inputs

T - Initial start time

TM - Time when maneuver starts

Target velocity is modeled by:

Z1 - Initial true position  
ZD - Time derivative  
T - Start time

IF (T .GE. TM) Z = Z + 0.5 x ZDD x (T-TM) \*\*2

(0.5 x ZDD x (T-TM)\*\*2) = Position change due to maneuver

### b. Noise Modeling

Subroutine GAUSS - Generates random numbers

GAUSS (NO, SIG, RMEAN, WG)

NO = Seed

SIG - Standard deviation

RMEAN = Desired mean of the normal distribution

WG = Value of the computed normal random variable

$Y = Z + WG$  (where Y = noisy position measurement)

### C. Logic

#### 1. Estimating Logic

$$\begin{aligned} \text{XBAR} &= \text{XHAT} + G \times (\text{Y}-\text{XHAT}) \\ \text{XDBAR} &= \text{XDHAT} + (H/\text{DELT}) \times (\text{Y}-\text{XHAT}) \\ \text{XDDBAR} &= \text{ZDDHAT} + ((2 \times K)/(\text{DELT}^2)) \times (\text{Y}-\text{XHAT}) \end{aligned}$$

#### 2. Predicting Logic

$$R = (\text{DELT}^2)/2.$$
$$\begin{aligned} \text{XHAT} &= \text{XBAR} + \text{XDBAR} \times \text{DELT} + \text{XDDBAR} \times R \\ \text{XDHAT} &= \text{XDBAR} + \text{XDDBAR} \times \text{DELT} \\ \text{XDDHAT} &= \text{XDDBAR} \end{aligned}$$

### III. RESULTS

Each value entered is repeated to provide the user with an opportunity to change or correct value(s). Moreover, one has the choice of printing detailed results for each step (Table 1), or a tabular summation of results (Table 2.)

Examples of inputs and corresponding results are shown in the figures that follow. For odd numbered figures, the time constant is 3. and DELT is .1, so BETA = .967216134.

### IV. SUMMARY AND CONCLUSION

This system shows how accurately a target can be tracked given the appropriate input values. Therefore, it is very important to use the initial values that will yield feasible results. Any change in the main program input values on pages 1 and 2 will change the results.

When BETA = .8 (even numbered figures), the program is able to track the displacement vectors fairly accurately. For example, in Figure 7, (BETA = .967) there was more lag in the result, but the curve was smoother. In Figure 8 (BETA = .8) it tracked more accurately, but there was more noise. The program was able to track the velocity vectors much better with a BETA of .967 as opposed to a BETA of .8. The results depend on how closely the initial filter states correspond to the true state values and on the filter damping design, which is determined by the choice of BETA.

TABLE 1. Detailed Step by Step Results

INPUT SECTION

\*\*\*\*\*

NAME OF OUTPUT IS DISP VECTOR NO NOISE NO MANEUVER

SEED FOR THIS RUN IS 1

XCAR= 10273.00 XBAR= -0.15000E+03 XDBAR= 0.00000E+00

THE VALUE OF BETA IS 0.967000008E+00

G= 0.9576393E-01 H= 0.3213094E-02 K= 0.1796342E-04

NOISE FACTOR IS 0.00 MEAN IS 0.00

Z1= 0.10000E+05 Z01= -0.30000E+03 Z00= 0.00000E+00

IMAX= 60

T= 0.00 DELT= 0.10 T\* = 10.00

\*\*\*\*\*

# RESULTS FOR STEP 1

T XBAR XDBAR XDDBAR  
0.10000E+00 0.10270E+03 -0.15000E+03 0.00000E+00

XHAT XDHAT XDDHAT  
0.10255E+03 -0.15000E+03 0.00000E+00

Z ZD ZDD  
0.99700E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
0.30000E+03 0.15000E+03 0.00000E+00

Y= 0.99700E+04 (Y-XHAT) = -0.22500E+03

# RESULTS FOR STEP 2

T XBAR XDBAR XDDBAR  
0.20000E+00 0.10225E+03 -0.16012E+03 -0.11320E+01

XHAT XDHAT XDDHAT  
0.10209E+03 -0.16023E+03 -0.11320E+01

Z ZD ZDD  
0.99400E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
0.20433E+03 0.13980E+03 -0.11320E+01

Y= 0.99400E+04 (Y-XHAT) = -0.26382E+03

# RESULTS FOR STEP 3

T XBAR XDBAR XDDBAR  
0.30000E+00 0.10130E+03 -0.16964E+03 -0.22059E+01

XHAT XDHAT XDDHAT  
0.10163E+03 -0.17000E+03 -0.22059E+01

Z ZD ZDD  
0.99100E+04 -0.30000E+03 0.00000E+00

$XBAR - Z$        $XDEAP-ZD$        $XDEAP-ZDD$   
 $0.27020E+03$      $0.13015E+03$      $-0.22059E+01$

$Y = 0.92100E+04$      $(Y-XHAT) = -0.25320E+03$

#### RESULTS FOR STEP 4

$T$        $XBAR$        $XDBAR$        $XDDBAR$   
 $0.40000E+00$      $0.10135E+03$      $-0.17916E+03$      $-0.32236E+01$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.10113E+03$      $-0.17945E+03$      $-0.32236E+01$

$Z$        $ZD$        $ZDD$   
 $0.90000E+04$      $-0.70000E+03$      $0.00000E+00$

$XBAR - Z$        $XDEAP-ZD$        $XDEAP-ZDD$   
 $0.25600E+03$      $0.12034E+03$      $-0.32236E+01$

$Y = 0.93600E+04$      $(Y-XHAT) = -0.23315E+03$

#### RESULTS FOR STEP 5

$T$        $XBAR$        $XDBAR$        $XDDBAR$   
 $0.50000E+00$      $0.10022E+03$      $-0.15009E+03$      $-0.41473E+01$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.10074E+03$      $-0.14951E+03$      $-0.41373E+01$

$Z$        $ZD$        $ZDD$   
 $0.24500E+04$      $-0.70000E+03$      $0.00000E+00$

$XBAR - Z$        $XDEAP-ZD$        $XDEAP-ZDD$   
 $0.24247E+03$      $0.11191E+03$      $-0.41373E+01$

$Y = 0.93500E+04$      $(Y-XHAT) = -0.22364E+03$

RESULTS FOR STEP 6

T XBAR XDBAR XDDBAR  
0.00000E+00 0.10049E+05 -0.19666E+03 -0.50988E+01

XHAT XDHAT XDDHAT  
0.10030E+05 -0.19717E+03 -0.50988E+01

Z ZD ZDD  
0.96200E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDHAR-ZD XDDBAR-ZDD  
0.22935E+03 0.10334E+03 -0.50988E+01

Y= 0.96200E+04 (Y-XHAT) = -0.20966E+03

RESULTS FOR STEP 7

T XBAR XDBAR XDDBAR  
0.70000E+00 0.10007E+05 -0.20487E+03 -0.59600E+01

XHAT XDHAT XDDHAT  
0.99362E+04 -0.20547E+03 -0.59600E+01

Z ZD ZDD  
0.97000E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDHAR-ZD XDDBAR-ZDD  
0.21571E+03 0.95127E+02 -0.59600E+01

Y= 0.97000E+04 (Y-XHAT) = -0.19519E+03

RESULTS FOR STEP 8

T XBAR XDBAR XDDBAR  
0.00000E+00 0.99645E+04 -0.21274E+03 -0.67729E+01

XHAT XDHAT XDDHAT  
0.99432E+04 -0.21341E+03 -0.67729E+01

Z	ZD	ZDD
0.97600E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
0.20453E+03	0.87064E+02	-0.67729E+01

Y= 0.97600E+04 (Y-XHAT) = -0.16322E+03

# RESULTS FOR STEP 9

T	XBAR	XDBAR	XDDBAR
0.90000E+00	0.99023E+04	-0.22036E+03	-0.75391E+01

XHAT	YD HAT	XDDHAT
0.99007E+04	-0.22103E+03	-0.75391E+01

Z	ZD	ZDD
0.97300E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
0.19230E+03	0.79735E+02	-0.75391E+01

Y= 0.97300E+04 (Y-XHAT) = -0.17073E+03

# RESULTS FOR STEP 10

T	XBAR	XDBAR	XDDBAR
0.10000E+01	0.73615E+04	-0.22747E+03	-0.92605E+01

XHAT	YD HAT	XDDHAT
0.96507E+04	-0.22000E+03	-0.92605E+01

Z	ZD	ZDD
0.97000E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
0.18151E+03	0.72632E+02	-0.92605E+01

Y= 0.97000E+04 (Y-XHAT) = -0.15672E+03

# RESULTS FOR STEP 11

T XBAR XDBAR XDDBAR  
0.11000E+01 0.96405E+04 -0.27436E+03 -0.39327E+01

XHAT XDHAT XDDHAT  
0.98172E+04 -0.23525E+03 -0.39337E+01

Z ZD ZDD  
0.96700E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
0.17065E+03 0.65642E+02 -0.09397E+01

Y = 0.96700E+04 (Y - XHAT) = -0.14717E+03

# RESULTS FOR STEP 12

T XBAR XDBAR XDDBAR  
0.12000E+01 0.93002E+04 -0.24094E+03 -0.95754E+01

XHAT XDHAT XDDHAT  
0.97761E+04 -0.24190E+03 -0.95754E+01

Z ZD ZDD  
0.96400E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
0.16020E+03 0.59035E+02 -0.95754E+01

Y = 0.96400E+04 (Y - XHAT) = -0.13600E+03

# RESULTS FOR STEP 13

T XBAR XDBAR XDDBAR  
0.13000E+01 0.97502E+04 -0.24724E+03 -0.10172E+02

XHAT XDHAT XDDHAT  
0.97354E+04 -0.24220E+03 -0.10170E+02

Z ZD ZDD  
0.96100E+04 -0.30000E+03 0.00000E+00



XBAR - Z	XBAR-ZD	XDBAR-ZDD
0.15015E+03	0.52762E+02	-0.10172E+02

Y= 0.95100E+04 (Y-XHAT) = -0.12530E+03

#### RESULTS FOR STEP 14

T	XBAR	XDBAR	XDDPAR
0.14000E+01	0.97205E+04	-0.25325E+03	-0.10731E+02

XHAT	XDHAT	XDDHAT
0.95951E+04	-0.25432E+03	-0.10731E+02

Z	ZD	ZDD
0.95600E+04	-0.20000E+03	0.00000E+00

XBAR - Z	XBAR-ZD	XDBAR-ZDD
0.14050E+03	0.46753E+02	-0.10731E+02

Y= 0.95600E+04 (Y-XHAT) = -0.11512E+03

#### RESULTS FOR STEP 15

T	XBAR	XDBAR	XDDPAR
0.15000E+01	0.96812E+04	-0.25698E+03	-0.11252E+02

XHAT	XDHAT	XDDHAT
0.95553E+04	-0.26011E+03	-0.11252E+02

Z	ZD	ZDD
0.95500E+04	-0.20000E+03	0.00000E+00

XBAR - Z	XBAR-ZD	XDBAR-ZDD
0.13122E+03	0.41017E+02	-0.11252E+02

Y= 0.95500E+04 (Y-XHAT) = -0.10527E+03

RESULTS FOR STEP 16

T XBAR XDBAR XDDBAR  
0.16000E+01 0.95423E+04 -0.26445E+03 -0.11738E+02

XHAT XDHAT XDDHAT  
0.96153E+04 -0.26363E+03 -0.11738E+02

Z ZD ZDD  
0.95200E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
0.12231E+03 0.35545E+02 -0.11738E+02

Y = 0.95200E+04 (Y - XHAT) = -0.95310E+02

RESULTS FOR STEP 17

T XBAR XDBAR XDDBAR  
0.17000E+01 0.96038E+04 -0.26967E+03 -0.12190E+02

XHAT XDHAT XDDHAT  
0.95767E+04 -0.27089E+03 -0.12190E+02

Z ZD ZDD  
0.94900E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
0.11375E+03 0.30329E+02 -0.12190E+02

Y = 0.94900E+04 (Y - XHAT) = -0.16733E+02

RESULTS FOR STEP 18

T XBAR XDBAR XDDBAR  
0.18000E+01 0.95656E+04 -0.27464E+03 -0.12610E+02

XHAT XDHAT XDDHAT  
0.95310E+04 -0.27590E+03 -0.12610E+02

Z ZD ZDD  
0.94900E+04 -0.30000E+03 0.00000E+00

$XBAR = Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $0.10555E+03$      $0.25357E+02$      $-0.12610E+02$

$Y = 0.94000E+04$      $(Y-XHAT) = -0.70020E+02$

# RESULTS FOR STEP 19

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.19000E+01$      $0.95277E+04$      $-0.27937E+03$      $-0.12998E+02$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.94997E+04$      $-0.23067E+03$      $-0.12998E+02$

$Z$        $ZD$        $ZDD$   
 $0.94500E+04$      $-0.30000E+03$      $0.00000E+00$

$XBAR = Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $0.97501E+02$      $0.20627E+02$      $-0.12998E+02$

$Y = 0.94300E+04$      $(Y-XHAT) = -0.69578E+02$

# RESULTS FOR STEP 20

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.20000E+01$      $0.94901E+04$      $-0.23338E+03$      $-0.13356E+02$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.94517E+04$      $-0.23521E+03$      $-0.13356E+02$

$Z$        $ZD$        $ZDD$   
 $0.94000E+04$      $-0.30000E+03$      $0.00000E+00$

$XBAR = Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $0.90132E+02$      $0.16125E+02$      $-0.13356E+02$

$Y = 0.94000E+04$      $(Y-XHAT) = -0.51673E+02$

# RESULTS FOR STEP 21

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.21000E+01$      $0.94302E+04$      $-0.23116E+03$      $-0.13666E+02$

XHAT XDHAT XDDHAT  
 0.94240E+04 -0.28953E+03 -0.13636E+02

Z ZD ZDD  
 0.93700E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR-ZD XDDBAR-ZDD  
 0.82597E+02 0.11843E+02 -0.13636E+02

Y= 0.93700E+04 (Y-XHAT) = -0.54014E+02

RESULTS FOR STEP 22

T XBAR XDBAR XDDBAR  
 0.22000E+01 0.94100E+04 -0.29222E+03 -0.13966E+02

XHAT XDHAT XDDHAT  
 0.93307E+04 -0.29362E+03 -0.13988E+02

Z ZD ZDD  
 0.93400E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR-ZD XDDBAR-ZDD  
 0.75958E+02 0.77753E+01 -0.13966E+02

Y= 0.93400E+04 (Y-XHAT) = -0.46675E+02

RESULTS FOR STEP 23

T XBAR XDBAR XDDBAR  
 0.25000E+01 0.93793E+04 -0.29802E+03 -0.14263E+02

XHAT XDHAT XDDHAT  
 0.93497E+04 -0.29751E+03 -0.14263E+02

Z ZD ZDD  
 0.93100E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR-ZD XDDBAR-ZDD  
 0.64332E+02 0.39102E+01 -0.14263E+02

Y= 0.93100E+04 (Y-XHAT) = -0.39652E+02

# RESULTS FOR STEP 24

T XBAR XDBAR XDBAR  
 0.24000E+01 0.93430E+04 -0.39975E+03 -0.14513E+02

XHAT XDHAT XDDHAT  
 0.93129E+04 -0.30120E+03 -0.14513E+02

Z ZD ZDD  
 0.92000E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR-ZD XDBAR-ZDD  
 0.92931E+02 0.24560E+00 -0.14513E+02

Y= 0.92500E+04 (Y-XHAT) = -0.32934E+02

# RESULTS FOR STEP 25

T XBAR XDBAR XDBAR  
 0.25000E+01 0.93069E+04 -0.30322E+03 -0.14740E+02

XHAT XDHAT XDDHAT  
 0.92765E+04 -0.30470E+03 -0.14740E+02

Z ZD ZDD  
 0.92500E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR-ZD XDBAR-ZDD  
 0.56906E+02 -0.32249E+01 -0.14740E+02

Y= 0.92500E+04 (Y-XHAT) = -0.26511E+02

# RESULTS FOR STEP 26

T XBAR XDBAR XDBAR  
 0.26000E+01 0.92711E+04 -0.30551E+03 -0.14943E+02

XHAT XDHAT XDDHAT  
 0.92404E+04 -0.30001E+03 -0.14943E+02

Z ZD ZDD  
 0.92000E+04 -0.30000E+03 0.00000E+00

XBAR - Z	XBAR-ZD	XDBAR-ZDD
0.51099E+02	-0.65145E+01	-0.14943E+02

Y= 0.92300E+04 (Y-XHAT) = -0.20372E+02

# RESULTS FOR STEP 27

T	XBAR	XDBAR	XDBAR
0.27000E+01	0.92355E+04	-0.30963E+03	-0.15124E+02

XHAT	XDHAT	XDDHAT
0.92045E+04	-0.31114E+03	-0.15124E+02

Z	ZD	ZDD
0.91900E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XBAR-ZD	XDBAR-ZDD
0.45548E+02	-0.96273E+01	-0.15124E+02

Y= 0.91900E+04 (Y-XHAT) = -0.14510E+02

# RESULTS FOR STEP 28

T	XBAR	XDBAR	XDBAR
0.28000E+01	0.92002E+04	-0.31257E+03	-0.15284E+02

XHAT	XDHAT	XDDHAT
0.91649E+04	-0.31410E+03	-0.15284E+02

Z	ZD	ZDD
0.91600E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XBAR-ZD	XDBAR-ZDD
0.40247E+02	-0.12570E+02	-0.15284E+02

Y= 0.91600E+04 (Y-XHAT) = -0.39141E+01

# RESULTS FOR STEP 29

T	XBAR	XDBAR	XDBAR
0.29000E+01	0.91552E+04	-0.31505E+03	-0.15404E+02

XHAT	XDHAT	XDDHAT
0.91336E+04	-0.31587E+03	-0.15424E+02

Z	ZD	ZDD
0.91300E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
0.35138E+02	-0.15349E+02	-0.15424E+02

Y= 0.91300E+04 (Y-XHAT) = -0.35752E+01

# RESULTS FOR STEP 10

T	XBAR	XDBAR	XDDBAR
0.30000E+01	0.91304E+04	-0.31797E+03	-0.15544E+02

XHAT	XDHAT	XDDHAT
0.90965E+04	-0.31952E+03	-0.15544E+02

Z	ZD	ZDD
0.91000E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
0.30359E+02	-0.17970E+02	-0.15544E+02

Y= 0.91000E+04 (Y-XHAT) = 0.15135E+01

# RESULTS FOR STEP 11

T	XBAR	XDBAR	XDDBAR
0.31000E+01	0.90955E+04	-0.32044E+03	-0.15647E+02

XHAT	XDHAT	XDDHAT
0.90635E+04	-0.32200E+03	-0.15647E+02

Z	ZD	ZDD
0.90700E+04	-0.30000E+03	0.00000E+00

$XBAR - Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $0.25757E+02$      $-0.20437E+02$      $-0.15647E+02$

$Y = 0.90700E+04$      $(Y-XHAT) = 0.63652E+01$

#### RESULTS FOR STEP 32

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.32000E+01$      $0.90514E+04$      $-0.32276E+03$      $-0.15731E+02$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.90290E+04$      $-0.32434E+03$      $-0.15731E+02$

$Z$        $ZD$        $ZDD$   
 $0.90400E+04$      $-0.30303E+03$      $0.00000E+00$

$XBAR - Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $0.21371E+02$      $-0.22763E+02$      $-0.15731E+02$

$Y = 0.90400E+04$      $(Y-XHAT) = 0.10384E+02$

#### RESULTS FOR STEP 33

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.33000E+01$      $0.90272E+04$      $-0.32495E+03$      $-0.15900E+02$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.89740E+04$      $-0.32653E+03$      $-0.15900E+02$

$Z$        $ZD$        $ZDD$   
 $0.90100E+04$      $-0.30000E+03$      $0.00000E+00$

$XBAR - Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $0.17174E+02$      $-0.24946E+02$      $-0.15800E+02$

$Y = 0.90100E+04$      $(Y-XHAT) = 0.15330E+02$

#### RESULTS FOR STEP 34

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.34000E+01$      $0.89432E+04$      $-0.32700E+03$      $-0.15953E+02$



XHAT	XDHAT	XDDHAT
0.39604E+04	-0.32853E+03	-0.15252E+02

Z	ZD	ZDD
0.89800E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDHAR-ZD	XDDBAR-ZDD
0.13220E+02	-0.26975E+02	-0.15352E+02

Y= 0.39600E+04 (Y-XHAT) = 0.19560E+02

# RESULTS FOR STEP 35

T	XBAR	XDHAR	XDDBAR
0.35000E+01	0.39594E+04	-0.32892E+03	-0.15690E+02

XHAT	XDHAT	XDDHAT
0.39205E+04	-0.33051E+03	-0.15390E+02

Z	ZD	ZDD
0.89500E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDHAR-ZD	XDDBAR-ZDD
0.94404E+01	-0.28913E+02	-0.15390E+02

Y= 0.39500E+04 (Y-XHAT) = 0.23500E+02

# RESULTS FOR STEP 36

T	XBAR	XDHAR	XDDBAR
0.36000E+01	0.39259E+04	-0.33071E+03	-0.15913E+02

XHAT	XDHAT	XDDHAT
0.38927E+04	-0.33231E+03	-0.15913E+02

Z	ZD	ZDD
0.39200E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
0.53500E+01	-0.30715E+02	-0.15913E+02

Y= 0.39200E+04 (Y-XHAT) = 0.27300E+02

# RESULTS FOR STEP 37

T	XBAR	XDBAR	XDDBAR
0.37000E+01	0.33724E+04	-0.33239E+03	-0.15923E+02

XHAT	XDHAT	XDDHAT
0.33591E+04	-0.33399E+03	-0.15923E+02

Z	ZD	ZDD
0.33900E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
0.24414E+01	-0.32393E+02	-0.15923E+02

Y= 0.33900E+04 (Y-XHAT) = 0.30876E+02

# RESULTS FOR STEP 38

T	XBAR	XDBAR	XDDBAR
0.38000E+01	0.33592E+04	-0.33396E+03	-0.15920E+02

XHAT	XDHAT	XDDHAT
0.33207E+04	-0.33553E+03	-0.15920E+02

Z	ZD	ZDD
0.38000E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.79492E+00	-0.33937E+02	-0.15920E+02

Y= 0.38000E+04 (Y-XHAT) = 0.54271E+02

# RESULTS FOR STEP 39

T XBAR XDBAR XDDBAR  
0.39000E+01 0.38261E+04 -0.33541E+03 -0.15904E+02

XHAT XDHAT XDDHAT  
0.37925E+04 -0.33700E+03 -0.15904E+02

Z ZD ZDD  
0.28300E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
-0.38513E+01 -0.35412E+02 -0.15904E+02

Y= 0.38300E+04 (Y-XHAT) = 0.37481E+02

# RESULTS FOR STEP 40

T XBAR XDBAR XDDBAR  
0.40000E+01 0.37932E+04 -0.33675E+03 -0.15877E+02

XHAT XDHAT XDDHAT  
0.37595E+04 -0.33835E+03 -0.15877E+02

Z ZD ZDD  
0.28300E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
-0.37545E+01 -0.35780E+02 -0.15877E+02

Y= 0.37900E+04 (Y-XHAT) = 0.40520E+02

# RESULTS FOR STEP 41

T XBAR XDBAR XDDBAR  
0.41000E+01 0.37605E+04 -0.33801E+03 -0.15840E+02

XHAT XDHAT XDDHAT  
0.37266E+04 -0.33960E+03 -0.15840E+02

Z ZD ZDD  
0.27700E+04 -0.30000E+03 0.00000E+00

$XBAR - Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $-0.95117E+01$     $-0.33012E+02$     $-0.15140E+02$

$Y = 0.27700E+04$     $(Y-XHAT) = 0.43392E+02$

#### RESULTS FOR STEP 42

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.42000E+01$     $0.7279E+04$     $-0.33917E+03$     $-0.15792E+02$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.86939E+04$     $-0.34074E+03$     $-0.15790E+02$

$Z$        $ZD$        $ZDD$   
 $0.87400E+04$     $-0.30000E+03$     $0.00000E+00$

$XBAR - Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $-0.12109E+02$     $-0.39165E+02$     $-0.15792E+02$

$Y = 0.87400E+04$     $(Y-XHAT) = 0.46105E+02$

#### RESULTS FOR STEP 43

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.43000E+01$     $0.6634E+04$     $-0.34023E+03$     $-0.15734E+02$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.85613E+04$     $-0.34100E+03$     $-0.15734E+02$

$Z$        $ZD$        $ZDD$   
 $0.67100E+04$     $-0.30000E+03$     $0.00000E+00$

$XBAR - Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $-0.14563E+02$     $-0.40227E+02$     $-0.15734E+02$

$Y = 0.67100E+04$     $(Y-XHAT) = 0.48656E+02$

#### RESULTS FOR STEP 44

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.44000E+01$     $0.6631E+04$     $-0.34170E+03$     $-0.15687E+02$

XHAT	XDHAT	XDDHAT
0.36289E+04	-0.34277E+03	-0.15667E+02

Z	ZD	ZDD
0.86800E+04	-0.30000E+03	0.00000E+00

X2AR - Z	XDEAR-ZD	XDDBAR-ZDD
-0.16378E+02	-0.41200E+02	-0.15667E+02

Y= 0.86800E+04 (Y-XHAT) = 0.51076E+02

RESULTS FOR STEP 45

T	XBAR	XDBAR	XDDBAR
0.45000E+01	0.36309E+04	-0.34219E+03	-0.15591E+02

XHAT	XDHAT	XDDHAT
0.35967E+04	-0.34365E+03	-0.15591E+02

Z	ZD	ZDD
0.36500E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDEAR-ZD	XDDBAR-ZDD
-0.19053E+02	-0.42090E+02	-0.15591E+02

Y= 0.36500E+04 (Y-XHAT) = 0.53345E+02

RESULTS FOR STEP 46

T	XBAR	XDBAR	XDDBAR
0.46000E+01	0.35439E+04	-0.34290E+03	-0.15507E+02

XHAT	XDHAT	XDDHAT
0.35645E+04	-0.34446E+03	-0.15507E+02

Z	ZD	ZDD
0.36200E+04	-0.30000E+03	0.00000E+00

$XBAR - Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $-0.21109E+02$     $-0.42899E+02$     $-0.15507E+02$

$Y = 0.26200E+04$      $(Y-XHAT) = 0.55477E+02$

#### RESULTS FOR STEP 47

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.47000E+01$     $0.05670E+04$     $-0.34363E+03$     $-0.15415E+02$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.35325E+04$     $-0.34517E+03$     $-0.15415E+02$

$Z$        $ZD$        $ZDD$   
 $0.55700E+04$     $-0.50000E+03$     $0.00000E+00$

$XBAR - Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $-0.23037E+02$     $-0.43631E+02$     $-0.15415E+02$

$Y = 0.25900E+04$      $(Y-XHAT) = 0.57473E+02$

#### RESULTS FOR STEP 48

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.48000E+01$     $0.05352E+04$     $-0.34429E+03$     $-0.15317E+02$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.35007E+04$     $-0.34512E+03$     $-0.15317E+02$

$Z$        $ZD$        $ZDD$   
 $0.55600E+04$     $-0.50000E+03$     $0.00000E+00$

$XBAR - Z$        $XBAR-ZD$        $XDBAR-ZDD$   
 $-0.24846E+02$     $-0.44290E+02$     $-0.15317E+02$

$Y = 0.55600E+04$      $(Y-XHAT) = 0.59351E+02$

#### RESULTS FOR STEP 49

$T$        $XBAR$        $XDBAR$        $XDBAR$   
 $0.49000E+01$     $0.05035E+04$     $-0.34445E+03$     $-0.15011E+02$

XHAT	XDHAT	XDDHAT
0.34669E+04	-0.34640E+03	-0.15211E+02

Z	ZD	ZDD
0.65300E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.26540E+02	-0.44676E+02	-0.15211E+02

Y= 0.65300E+04 (Y-XHAT) = 0.61104E+02

# RESULTS FOR STEP 50

T	XBAR	XDBAR	XDDBAR
0.50000E+01	0.34719E+04	-0.34540E+03	-0.15099E+02

XHAT	XDHAT	XDDHAT
0.34373E+04	-0.34591E+03	-0.15099E+02

Z	ZD	ZDD
0.65000E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.23126E+02	-0.45400E+02	-0.15099E+02

Y= 0.65000E+04 (Y-XHAT) = 0.62741E+02

# RESULTS FOR STEP 51

T	XBAR	XDBAR	XDDBAR
0.51000E+01	0.34404E+04	-0.34516E+03	-0.14982E+02

XHAT	XDHAT	XDDHAT
0.34057E+04	-0.34735E+03	-0.14982E+02

Z	ZD	ZDD
0.64700E+04	-0.30000E+03	0.00000E+00

$XBAR = Z$        $XDBAR-ZD$        $XDDBAR-ZDD$   
 $-0.29605E+02$      $-0.45355E+03$      $-0.14942E+02$

$Y = 0.34700E+04$      $(Y-XHAT) = 0.64267E+02$

# RESULTS FOR STEP 52

$T$        $XBAR$        $XDBAR$        $XDDBAR$   
 $0.52000E+01$      $0.34090E+04$      $-0.34626E+03$      $-0.14359E+02$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.53743E+04$      $-0.34774E+03$      $-0.14359E+02$

$Z$        $ZD$        $ZDD$   
 $0.34400E+04$      $-0.30000E+03$      $0.00000E+00$

$XBAR = Z$        $XDBAR-ZD$        $XDDBAR-ZDD$   
 $-0.30735E+02$      $-0.46235E+02$      $-0.14359E+02$

$Y = 0.34400E+04$      $(Y-XHAT) = 0.65666E+02$

# RESULTS FOR STEP 53

$T$        $XBAR$        $XDBAR$        $XDDBAR$   
 $0.53000E+01$      $0.33777E+04$      $-0.34659E+03$      $-0.14730E+02$

$XHAT$        $XDHAT$        $XDDHAT$   
 $0.33430E+04$      $-0.34007E+03$      $-0.14730E+02$

$Z$        $ZD$        $ZDD$   
 $0.34100E+04$      $-0.30000E+03$      $0.00000E+00$

$XBAR = Z$        $XDBAR-ZD$        $XDDBAR-ZDD$   
 $-0.32269E+02$      $-0.46394E+02$      $-0.14730E+02$

$Y = 0.34100E+04$      $(Y-XHAT) = 0.67000E+02$

# RESULTS FOR STEP 54

$T$        $XBAR$        $XDBAR$        $XDDBAR$   
 $0.54000E+01$      $0.33455E+04$      $-0.34613E+03$      $-0.14597E+02$



XHAT	XDHAT	XDDHAT
0.93113E+04	-0.34834E+03	-0.14597E+02

Z	ZD	ZDD
0.33300E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.33457E+02	-0.46679E+02	-0.14597E+02

Y= 0.33300E+04 (Y-XHAT) = 0.63218E+02

# RESULTS FOR STEP 55

T	XBAR	XDBAR	XDDBAR
0.55000E+01	0.83154E+04	-0.34711E+03	-0.14460E+02

XHAT	XDHAT	XDDHAT
0.82307E+04	-0.34855E+03	-0.14460E+02

Z	ZD	ZDD
0.33500E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.34558E+02	-0.47110E+02	-0.14450E+02

Y= 0.83500E+04 (Y-XHAT) = 0.59341E+02

# RESULTS FOR STEP 56

T	XBAR	XDBAR	XDDBAR
0.56000E+01	0.83064E+04	-0.34729E+03	-0.14319E+02

XHAT	XDHAT	XDDHAT
0.82496E+04	-0.34872E+03	-0.14319E+02

Z	ZD	ZDD
0.33200E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.35573E+02	-0.47292E+02	-0.14319E+02

$$Y = 0.63200E+04 \quad (Y-XHAT) = 0.70374E+02$$

# RESULTS FOR STEP 57

$$\begin{array}{cccc} T & XBAR & XDBAR & XDDBAR \\ 0.57000E+01 & 0.82535E+04 & -0.34745E+03 & -0.14174E+02 \end{array}$$

$$\begin{array}{ccc} XHAT & XDHAT & XDDHAT \\ 0.82137E+04 & -0.34884E+03 & -0.14174E+02 \end{array}$$

$$\begin{array}{ccc} Z & ZD & ZDD \\ 0.52900E+04 & -0.30000E+03 & 0.00000E+00 \end{array}$$

$$\begin{array}{ccc} XBAR - Z & XDBAR - ZD & XDDBAR - ZDD \\ -0.35500E+02 & -0.47427E+02 & -0.14174E+02 \end{array}$$

$$Y = 0.62000E+04 \quad (Y-XHAT) = 0.71022E+02$$

# RESULTS FOR STEP 58

$$\begin{array}{cccc} T & XBAR & XDBAR & XDDBAR \\ 0.58000E+01 & 0.82262E+04 & -0.34750E+03 & -0.14025E+02 \end{array}$$

$$\begin{array}{ccc} XHAT & XDHAT & XDDHAT \\ 0.81573E+04 & -0.34892E+03 & -0.14025E+02 \end{array}$$

$$\begin{array}{ccc} Z & ZD & ZDD \\ 0.82600E+04 & -0.30000E+03 & 0.00000E+00 \end{array}$$

$$\begin{array}{ccc} XBAR - Z & XDBAR - ZD & XDDBAR - ZDD \\ -0.37305E+02 & -0.47817E+02 & -0.14025E+02 \end{array}$$

$$Y = 0.62000E+04 \quad (Y-XHAT) = 0.72157E+02$$

# RESULTS FOR STEP 59

T XBAR XDBAR XDDBAR  
0.59000E+01 0.81719E+04 -0.34756E+03 -0.13873E+02

XHAT XDHAT XDDHAT  
0.81570E+04 -0.34895E+03 -0.13873E+02

Z ZC ZDC  
0.82300E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZC XDDBAR - ZDC  
-0.38147E+02 -0.47564E+02 -0.13873E+02

Y= 0.82300E+04 (Y-XHAT) = 0.72973E+02

# RESULTS FOR STEP 60

T XBAR XDBAR XDDBAR  
0.60000E+01 0.81611E+04 -0.34757E+03 -0.13719E+02

XHAT XDHAT XDDHAT  
0.81263E+04 -0.34894E+03 -0.13719E+02

Z ZC ZDC  
0.82000E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZC XDDBAR - ZDC  
-0.36357E+02 -0.47570E+02 -0.13719E+02

Y= 0.82000E+04 (Y-XHAT) = 0.73636E+02

# RESULTS FOR STEP 61

T XBAR XDBAR XDDBAR  
0.61000E+01 0.81303E+04 -0.34754E+03 -0.13562E+02

XHAT XDHAT XDDHAT  
0.80957E+04 -0.34890E+03 -0.13562E+02

Z	ZD	ZDD
0.01700E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.39499E+02	-0.47533E+02	-0.13562E+02

Y= 0.81700E+04 (Y-XHAT) = 0.74321E+02

# RESULTS FOR STEP 52

T	XBAR	XDBAR	XDDBAR
0.62000E+01	0.80999E+04	-0.34747E+03	-0.13403E+02

XHAT	XDHAT	XDDHAT
0.30651E+04	-0.34151E+03	-0.13403E+02

Z	ZD	ZDD
0.31400E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.40076E+02	-0.47471E+02	-0.13403E+02

Y= 0.31400E+04 (Y-XHAT) = 0.74090E+02

# RESULTS FOR STEP 53

T	XBAR	XDBAR	XDDBAR
0.63000E+01	0.8094E+04	-0.34737E+03	-0.13241E+02

XHAT	XDHAT	XDDHAT
0.30346E+04	-0.34169E+03	-0.13241E+02

Z	ZD	ZDD
0.31100E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.40591E+02	-0.47351E+02	-0.13241E+02

Y= 0.31100E+04 (Y-XHAT) = 0.75394E+02

# RESULTS FOR STEP 54

T XBAR XDBAR XDDBAR  
 $0.64000E+01$   $0.30300E+04$   $-0.34723E+03$   $-0.13075E+02$

XHAT XDHAT XDDHAT  
 $0.30042E+04$   $-0.34854E+03$   $-0.13075E+02$

Z ZD ZDD  
 $0.80000E+04$   $-0.30000E+03$   $0.00000E+00$

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
 $-0.41047E+02$   $-0.47234E+02$   $-0.13075E+02$

Y =  $0.30000E+04$  (Y - XHAT) =  $0.75336E+02$

# RESULTS FOR STEP 55

T XBAR XDBAR XDDBAR  
 $0.65000E+01$   $0.30036E+04$   $-0.34707E+03$   $-0.12914E+02$

XHAT XDHAT XDDHAT  
 $0.79733E+04$   $-0.34335E+03$   $-0.12914E+02$

Z ZD ZDD  
 $0.80500E+04$   $-0.30000E+03$   $0.00000E+00$

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
 $-0.41443E+02$   $-0.47007E+02$   $-0.12914E+02$

Y =  $0.30500E+04$  (Y - XHAT) =  $0.76213E+02$

# RESULTS FOR STEP 56

T XBAR XDBAR XDDBAR  
 $0.66000E+01$   $0.79782E+04$   $-0.34593E+03$   $-0.12747E+02$

XHAT XDHAT XDDHAT  
 $0.79435E+04$   $-0.34015E+03$   $-0.12747E+02$

Z	ZD	ZDD
0.80200E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.41792E+02	-0.46675E+02	-0.12747E+02

Y= 0.80200E+04 (Y-XHAT) = 0.76543E+02

# RESULTS FOR STEP 67

T	XBAR	XDBAR	XDDBAR
0.67700E+01	0.79479E+04	-0.34665E+03	-0.12550E+02

XHAT	XDHAT	XDDHAT
0.79132E+04	-0.34791E+03	-0.12500E+02

Z	ZD	ZDD
0.79900E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.42000E+02	-0.46655E+02	-0.12580E+02

Y= 0.79900E+04 (Y-XHAT) = 0.76314E+02

# RESULTS FOR STEP 68

T	XBAR	XDBAR	XDDBAR
0.68000E+01	0.79177E+04	-0.34641E+03	-0.12412E+02

XHAT	XDHAT	XDDHAT
0.79130E+04	-0.34705E+03	-0.12410E+02

Z	ZD	ZDD
0.79000E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.42331E+02	-0.46407E+02	-0.12412E+02

Y= 0.79000E+04 (Y-XHAT) = 0.77074E+02

RESULTS FOR STEP 69

T XBAR XDBAR XDDBAR  
0.59000E+01 0.78875E+04 -0.34614E+03 -0.12243E+02

XHAT XDHAT XDDHAT  
0.78528E+04 -0.34736E+03 -0.12243E+02

Z ZD ZDD  
0.79300E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
-0.40529E+02 -0.46139E+02 -0.12243E+02

Y= 0.79300E+04 (Y-XHAT) = 0.77204E+00

RESULTS FOR STEP 70

T XBAR XDBAR XDDBAR  
0.70000E+01 0.75573E+04 -0.34535E+03 -0.12073E+02

XHAT XDHAT XDDHAT  
0.78227E+04 -0.34705E+03 -0.12073E+02

Z ZD ZDD  
0.79000E+04 -0.30000E+03 0.00000E+00

XBAR - Z XDBAR - ZD XDDBAR - ZDD  
-0.42574E+02 -0.45146E+02 -0.12073E+02

Y= 0.79000E+04 (Y-XHAT) = 0.77724E+00

RESULTS FOR STEP 71

T XBAR XDBAR XDDBAR  
0.71000E+01 0.75272E+04 -0.34553E+03 -0.11903E+02

XHAT XDHAT XDDHAT  
0.77900E+04 -0.34670E+03 -0.11903E+02

Z	ZD	ZDD
0.72700E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.42796E+02	-0.45533E+02	-0.11903E+02

Y= 0.73700E+04 (Y-XHAT) = 0.77409E+02

# RESULTS FOR STEP 72

T	XBAR	XDBAR	XDDBAR
0.72000E+01	0.77971E+04	-0.34520E+03	-0.11733E+02

XHAT	ADHAT	XDDHAT
0.77526E+04	-0.34537E+03	-0.11733E+02

Z	ZD	ZDD
0.73400E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.42869E+02	-0.45200E+02	-0.11733E+02

Y= 0.73400E+04 (Y-XHAT) = 0.77447E+02

# RESULTS FOR STEP 73

T	XBAR	XDBAR	XDDBAR
0.73000E+01	0.77671E+04	-0.34435E+03	-0.11562E+02

XHAT	ADHAT	XDDHAT
0.77526E+04	-0.34500E+03	-0.11562E+02

Z	ZD	ZDD
0.73100E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.42933E+02	-0.44049E+02	-0.11562E+02

Y= 0.73100E+04 (Y-XHAT) = 0.77445E+02



# RESULTS FOR STEP 74

T                      XBAR                      XDBAR                      XDDBAR  
0.74000E+01    0.77371E+04    -0.34442E+03    -0.11392E+02

XHAT                      XDHAT                      XDDHAT  
0.77026E+04    -0.34562E+03    -0.11392E+02

Z                      ZD                      ZDD  
0.77000E+04    -0.30000E+03    0.00000E+00

XBAR - Z                      XDBAR - ZD                      XDDBAR - ZDD  
-0.42902E+02    -0.44480E+02    -0.11392E+02

Y = 0.77300E+04    (Y - XHAT) = 0.77407E+02

# RESULTS FOR STEP 75

T                      XBAR                      XDBAR                      XDDBAR  
0.75000E+01    0.77371E+04    -0.34410E+03    -0.11221E+02

XHAT                      XDHAT                      XDDHAT  
0.76727E+04    -0.34522E+03    -0.11221E+02

Z                      ZD                      ZDD  
0.77500E+04    -0.30000E+03    0.00000E+00

XBAR - Z                      XDBAR - ZD                      XDDBAR - ZDD  
-0.42367E+02    -0.44096E+02    -0.11221E+02

Y = 0.77500E+04    (Y - XHAT) = 0.77533E+02

# RESULTS FOR STEP 76

T                      XBAR                      XDBAR                      XDDBAR  
0.76000E+01    0.76772E+04    -0.34370E+03    -0.11051E+02

XHAT                      XDHAT                      XDDHAT  
0.76403E+04    -0.34480E+03    -0.11051E+02

Z	ZD	ZDD
0.77200E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.42300E+02	-0.43695E+02	-0.11051E+02

Y= 0.77200E+04 (Y-XHAT) = 0.77235E+02

#### RESULTS FOR STEP 77

T	XBAR	XDBAR	XDDBAR
0.77000E+01	0.76473E+04	-0.34329E+03	-0.10882E+02

XHAT	XDHAT	XDDHAT
0.76129E+04	-0.34437E+03	-0.10882E+02

Z	ZD	ZDD
0.76900E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.42702E+02	-0.43085E+02	-0.10882E+02

Y= 0.76900E+04 (Y-XHAT) = 0.77095E+02

#### RESULTS FOR STEP 78

T	XBAR	XDBAR	XDDBAR
0.76000E+01	0.76174E+04	-0.34285E+03	-0.10712E+02

XHAT	XDHAT	XDDHAT
0.75331E+04	-0.34393E+03	-0.10712E+02

Z	ZD	ZDD
0.75600E+04	-0.30000E+03	0.00000E+00

XBAR - Z	XDBAR-ZD	XDDBAR-ZDD
-0.42576E+02	-0.42861E+02	-0.10712E+02

Y= 0.75600E+04 (Y-XHAT) = 0.75916E+02

RESULTS FOR STEP 79

T                    XBAR                    XDBAR                    XDDBAR  
 0.79000E+01    0.75575E+04    -0.34242E+03    -0.10544E+02

XHAT                    XDHAT                    XDDHAT  
 0.75533E+04    -0.34343E+03    -0.10544E+02

Z                    ZD                    ZDD  
 0.76300E+04    -0.30000E+03    0.00000E+00

XBAR - Z                    XDBAR-ZD                    XDDBAR-ZDD  
 -0.42422E+02    -0.42424E+02    -0.10544E+02

Y= 0.76300E+04    (Y-XHAT) = 0.76715E+02

RESULTS FOR STEP 80

T                    XBAR                    XDBAR                    XDDBAR  
 0.80000E+01    0.75575E+04    -0.34195E+03    -0.10376E+02

XHAT                    XDHAT                    XDDHAT  
 0.75235E+04    -0.34300E+03    -0.10376E+02

Z                    ZD                    ZDD  
 0.76000E+04    -0.30000E+03    0.00000E+00

XBAR - Z                    XDBAR-ZD                    XDDBAR-ZDD  
 -0.42244E+02    -0.41975E+02    -0.10376E+02

Y= 0.76000E+04    (Y-XHAT) = 0.76493E+02

TABLE 2. Tabular Summation

```

*****
      INPUT SECTION
*****
NAME OF OUTPUT IS DISP VECTOR (NO NOISE, NO MANEUVER) - BETA = .967
SEED FOR THIS RUN IS      1

      XBAR= 10270.00 XDBAR= -0.15000E+03 XDDBAR= 0.00000E+00
      NOISE FACTOR IS 0.00 MEAN IS 0.00
      Z1= 0.10000E+05 Z01= -0.30000E+03 ZDD= 0.00000E+00
      IMAX= 80
      T= 0.00 DELT= 0.10 TM= 10.00
*****

```

STEP	Z	XBAR	ZD	XDRAP	ZDD	XDDBAR
1	0.99700E+04	0.10270E+05	-0.30000E+03	-0.15000E+03	0.00000E+00	0.00000E+00
2	0.99400E+04	0.10225E+05	-0.30000E+03	-0.16012E+03	0.00000E+00	-0.11320E+01
3	0.99100E+04	0.10130E+05	-0.30000E+03	-0.16984E+03	0.00000E+00	-0.22059E+01
4	0.98800E+04	0.10136E+05	-0.30000E+03	-0.17916E+03	0.00000E+00	-0.32236E+01
5	0.98500E+04	0.10091E+05	-0.30000E+03	-0.18809E+03	0.00000E+00	-0.41873E+01
6	0.98200E+04	0.10049E+05	-0.30000E+03	-0.19666E+03	0.00000E+00	-0.50988E+01
7	0.97900E+04	0.10007E+05	-0.30000E+03	-0.20487E+03	0.00000E+00	-0.59600E+01
8	0.97600E+04	0.99645E+04	-0.30000E+03	-0.21274E+03	0.00000E+00	-0.67729E+01
9	0.97300E+04	0.99223E+04	-0.30000E+03	-0.22026E+03	0.00000E+00	-0.75391E+01
10	0.97000E+04	0.98815E+04	-0.30000E+03	-0.22747E+03	0.00000E+00	-0.82605E+01
11	0.96700E+04	0.98406E+04	-0.30000E+03	-0.23436E+03	0.00000E+00	-0.89387E+01
12	0.96400E+04	0.98001E+04	-0.30000E+03	-0.24094E+03	0.00000E+00	-0.95754E+01

STEP	Z	XBAR	ZD	XBAR	ZDD	XDDBAR
13	0.96100E+04	0.97602E+04	-0.30000E+03	-0.24724E+03	0.00000E+00	-0.10172E+02
14	0.95800E+04	0.97205E+04	-0.30000E+03	-0.25325E+03	0.00000E+00	-0.10731E+02
15	0.95500E+04	0.96812E+04	-0.30000E+03	-0.25898E+03	0.00000E+00	-0.11252E+02
16	0.95200E+04	0.96423E+04	-0.30000E+03	-0.26445E+03	0.00000E+00	-0.11738E+02
17	0.94900E+04	0.96032E+04	-0.30000E+03	-0.26967E+03	0.00000E+00	-0.12190E+02
18	0.94600E+04	0.95655E+04	-0.30000E+03	-0.27464E+03	0.00000E+00	-0.12610E+02
19	0.94300E+04	0.95277E+04	-0.30000E+03	-0.27937E+03	0.00000E+00	-0.12998E+02
20	0.94000E+04	0.94901E+04	-0.30000E+03	-0.28398E+03	0.00000E+00	-0.13356E+02
21	0.93700E+04	0.94529E+04	-0.30000E+03	-0.28916E+03	0.00000E+00	-0.13686E+02
22	0.93400E+04	0.94160E+04	-0.30000E+03	-0.29222E+03	0.00000E+00	-0.13986E+02
23	0.93100E+04	0.93793E+04	-0.30000E+03	-0.29609E+03	0.00000E+00	-0.14263E+02
24	0.92800E+04	0.93470E+04	-0.30000E+03	-0.29975E+03	0.00000E+00	-0.14513E+02
25	0.92500E+04	0.93100E+04	-0.30000E+03	-0.30322E+03	0.00000E+00	-0.14740E+02

STEP	Z	XBAR	ZD	XDBAR	ZDD	XDDBAR
26	0.92200E+04	0.92711E+04	-0.30000E+03	-0.30651E+03	0.00000E+00	-0.14943E+02
27	0.91900E+04	0.92355E+04	-0.30000E+03	-0.30963E+03	0.00000E+00	-0.15124E+02
28	0.91600E+04	0.92000E+04	-0.30000E+03	-0.31257E+03	0.00000E+00	-0.15284E+02
29	0.91300E+04	0.91652E+04	-0.30000E+03	-0.31535E+03	0.00000E+00	-0.15424E+02
30	0.91000E+04	0.91304E+04	-0.30000E+03	-0.31797E+03	0.00000E+00	-0.15544E+02
31	0.90700E+04	0.90955E+04	-0.30000E+03	-0.32044E+03	0.00000E+00	-0.15647E+02
32	0.90400E+04	0.90614E+04	-0.30000E+03	-0.32276E+03	0.00000E+00	-0.15731E+02
33	0.90100E+04	0.90272E+04	-0.30000E+03	-0.32495E+03	0.00000E+00	-0.15800E+02
34	0.89800E+04	0.89932E+04	-0.30000E+03	-0.32700E+03	0.00000E+00	-0.15852E+02
35	0.89500E+04	0.89594E+04	-0.30000E+03	-0.32892E+03	0.00000E+00	-0.15890E+02
36	0.89200E+04	0.89257E+04	-0.30000E+03	-0.33071E+03	0.00000E+00	-0.15913E+02
37	0.88900E+04	0.88924E+04	-0.30000E+03	-0.33239E+03	0.00000E+00	-0.15923E+02

STEP	Z	XBAR	ZD	XDBAR	ZDD	XDDBAR
38	0.88600E+04	0.28592E+04	-0.30000E+03	-0.33396E+03	0.00000E+00	-0.15920E+02
39	0.88300E+04	0.59261E+04	-0.30000E+03	-0.33541E+03	0.00000E+00	-0.15904E+02
40	0.88000E+04	0.67532E+04	-0.30000E+03	-0.33676E+03	0.00000E+00	-0.15877E+02
41	0.87700E+04	0.57605E+04	-0.30000E+03	-0.33801E+03	0.00000E+00	-0.15840E+02
42	0.87400E+04	0.67279E+04	-0.30000E+03	-0.33917E+03	0.00000E+00	-0.15792E+02
43	0.87100E+04	0.66954E+04	-0.30000E+03	-0.34023E+03	0.00000E+00	-0.15734E+02
44	0.86800E+04	0.66631E+04	-0.30000E+03	-0.34120E+03	0.00000E+00	-0.15667E+02
45	0.86500E+04	0.66309E+04	-0.30000E+03	-0.34209E+03	0.00000E+00	-0.15591E+02
46	0.86200E+04	0.65984E+04	-0.30000E+03	-0.34290E+03	0.00000E+00	-0.15507E+02
47	0.85900E+04	0.65670E+04	-0.30000E+03	-0.34363E+03	0.00000E+00	-0.15415E+02
48	0.85600E+04	0.65352E+04	-0.30000E+03	-0.34429E+03	0.00000E+00	-0.15317E+02
49	0.85300E+04	0.65033E+04	-0.30000E+03	-0.34473E+03	0.00000E+00	-0.15211E+02
50	0.85000E+04	0.64713E+04	-0.30000E+03	-0.34540E+03	0.00000E+00	-0.15099E+02



STEP	Z	XBAR	ZD	XDBAR	XDD	XDDBAR
51	0.84700E+04	0.84404E+04	-0.30000E+03	-0.34536E+03	0.00000E+00	-0.14982E+02
52	0.84400E+04	0.84090E+04	-0.30000E+03	-0.34626E+03	0.00000E+00	-0.14859E+02
53	0.84100E+04	0.83777E+04	-0.30000E+03	-0.34659E+03	0.00000E+00	-0.14730E+02
54	0.83800E+04	0.83465E+04	-0.30000E+03	-0.34689E+03	0.00000E+00	-0.14597E+02
55	0.83500E+04	0.83154E+04	-0.30000E+03	-0.34711E+03	0.00000E+00	-0.14460E+02
56	0.83200E+04	0.82844E+04	-0.30000E+03	-0.34729E+03	0.00000E+00	-0.14319E+02
57	0.82900E+04	0.82535E+04	-0.30000E+03	-0.34743E+03	0.00000E+00	-0.14174E+02
58	0.82600E+04	0.82225E+04	-0.30000E+03	-0.34752E+03	0.00000E+00	-0.14025E+02
59	0.82300E+04	0.81914E+04	-0.30000E+03	-0.34756E+03	0.00000E+00	-0.13873E+02
60	0.82000E+04	0.81611E+04	-0.30000E+03	-0.34757E+03	0.00000E+00	-0.13719E+02
61	0.81700E+04	0.81305E+04	-0.30000E+03	-0.34754E+03	0.00000E+00	-0.13562E+02
62	0.81400E+04	0.80999E+04	-0.30000E+03	-0.34747E+03	0.00000E+00	-0.13403E+02
63	0.81100E+04	0.80674E+04	-0.30000E+03	-0.34737E+03	0.00000E+00	-0.13241E+02

STEP	Z	XBAR	ZD	XDBAR	ZDD	XDDBAR
64	0.80800E+04	0.80390E+04	-0.30000E+03	-0.34723E+03	0.00000E+00	-0.13078E+02
65	0.80500E+04	0.80080E+04	-0.30000E+03	-0.34707E+03	0.00000E+00	-0.12914E+02
66	0.80200E+04	0.79782E+04	-0.30000E+03	-0.34688E+03	0.00000E+00	-0.12747E+02
67	0.79900E+04	0.79473E+04	-0.30000E+03	-0.34665E+03	0.00000E+00	-0.12580E+02
68	0.79600E+04	0.79177E+04	-0.30000E+03	-0.34641E+03	0.00000E+00	-0.12412E+02
69	0.79300E+04	0.78755E+04	-0.30000E+03	-0.34614E+03	0.00000E+00	-0.12243E+02
70	0.79000E+04	0.78573E+04	-0.30000E+03	-0.34585E+03	0.00000E+00	-0.12073E+02
71	0.78700E+04	0.78272E+04	-0.30000E+03	-0.34553E+03	0.00000E+00	-0.11903E+02
72	0.78400E+04	0.77971E+04	-0.30000E+03	-0.34520E+03	0.00000E+00	-0.11733E+02
73	0.78100E+04	0.77771E+04	-0.30000E+03	-0.34485E+03	0.00000E+00	-0.11562E+02
74	0.77800E+04	0.77571E+04	-0.30000E+03	-0.34443E+03	0.00000E+00	-0.11392E+02
75	0.77500E+04	0.77371E+04	-0.30000E+03	-0.34410E+03	0.00000E+00	-0.11221E+02

STEP	Z	XBAR	ZD°	XDBAR	ZDD	XDDBAR
76	0.77200E+04	0.76772E+04	-0.30000E+03	-0.34370E+03	0.00000E+00	-0.11051E+02
77	0.76900E+04	0.76473E+04	-0.30000E+03	-0.34329E+03	0.00000E+00	-0.10882E+02
78	0.76600E+04	0.76174E+04	-0.30000E+03	-0.34286E+03	0.00000E+00	-0.10712E+02
79	0.76300E+04	0.75875E+04	-0.30000E+03	-0.34242E+03	0.00000E+00	-0.10544E+02
80	0.76000E+04	0.75575E+04	-0.30000E+03	-0.34198E+03	0.00000E+00	-0.10376E+02

END OF JOB FOR PROGRAM DISP VECTOR (NO NOISE, NO MANEUVER) - BETA = .967

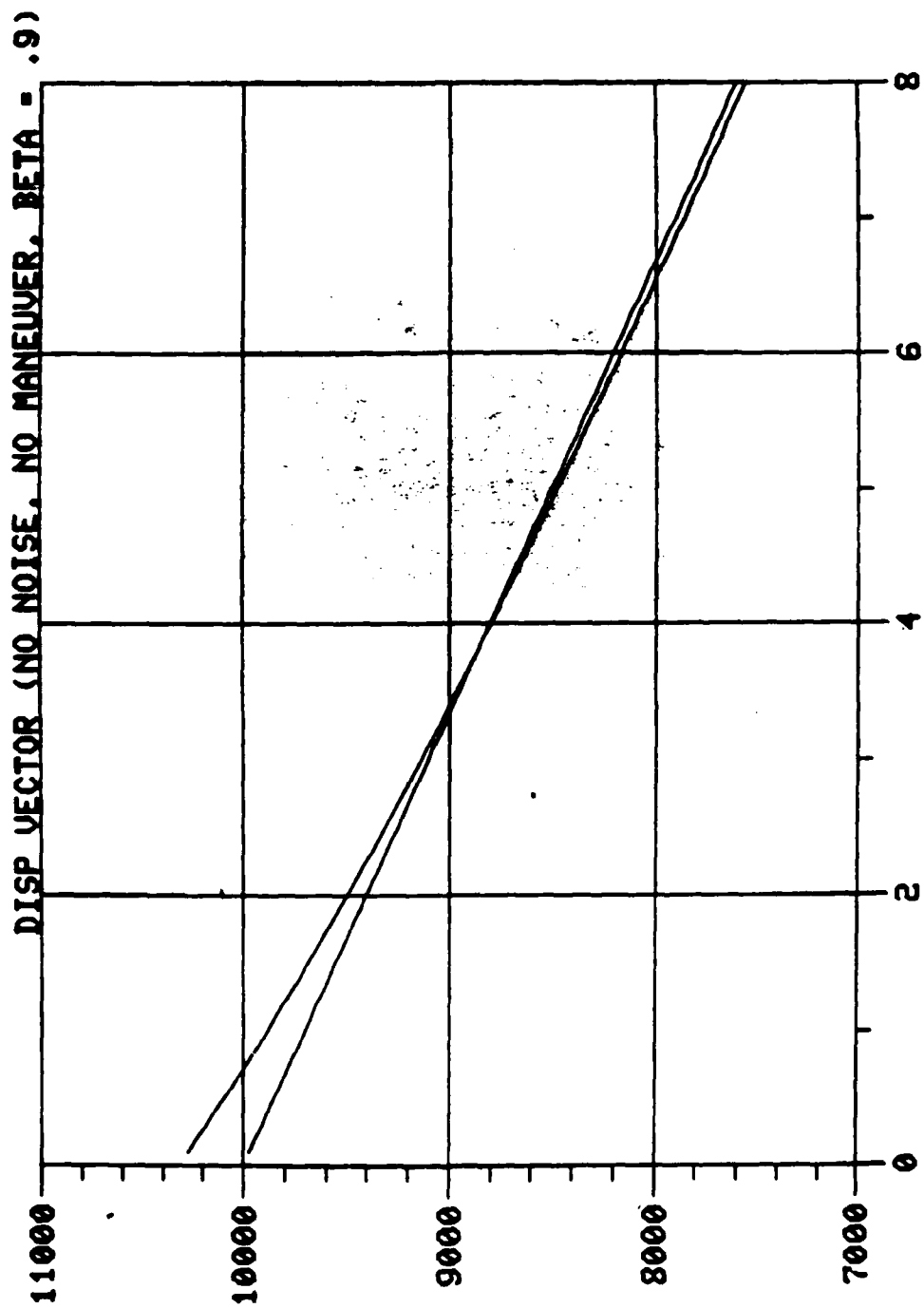


Figure 1

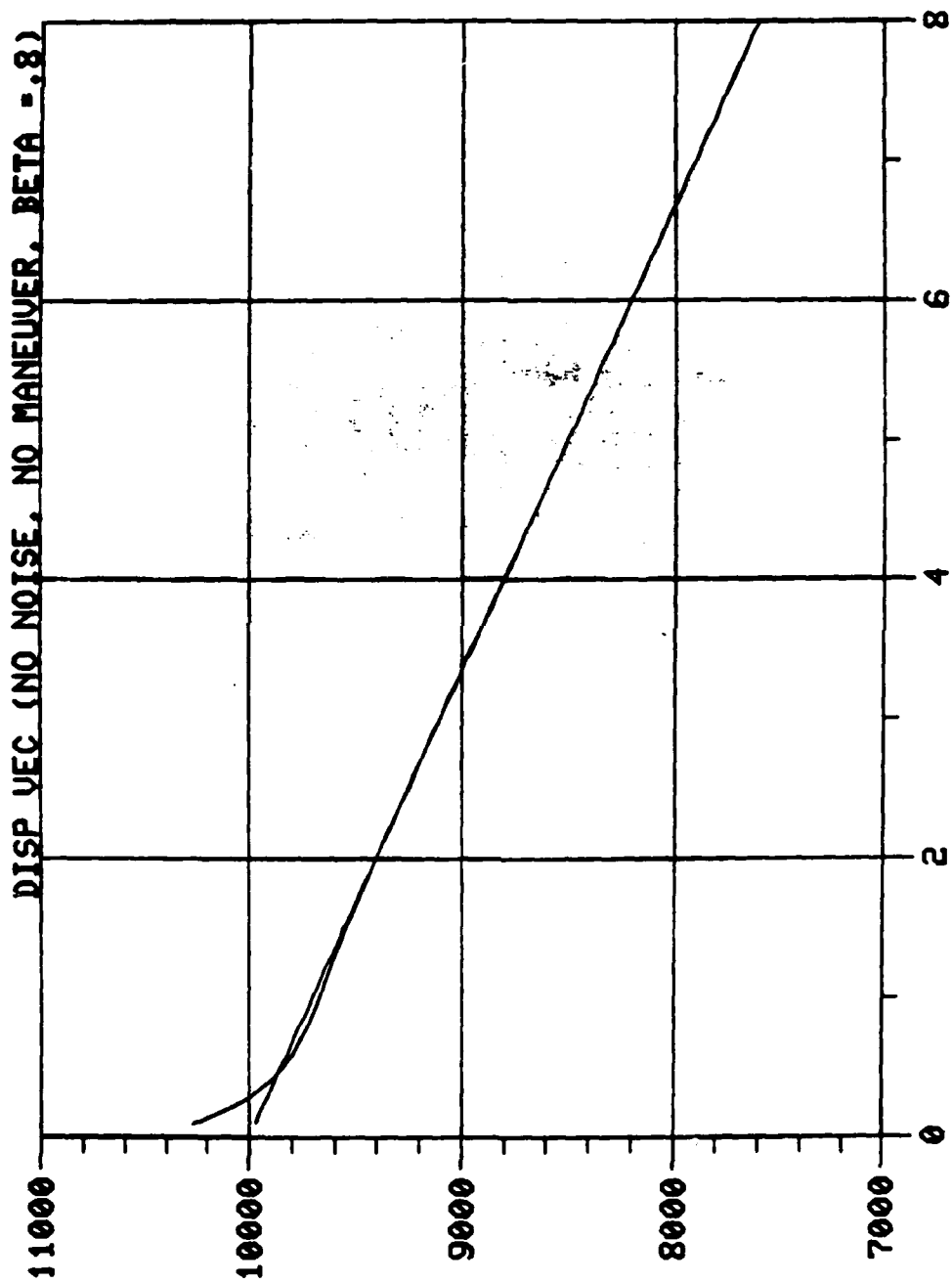


Figure 2

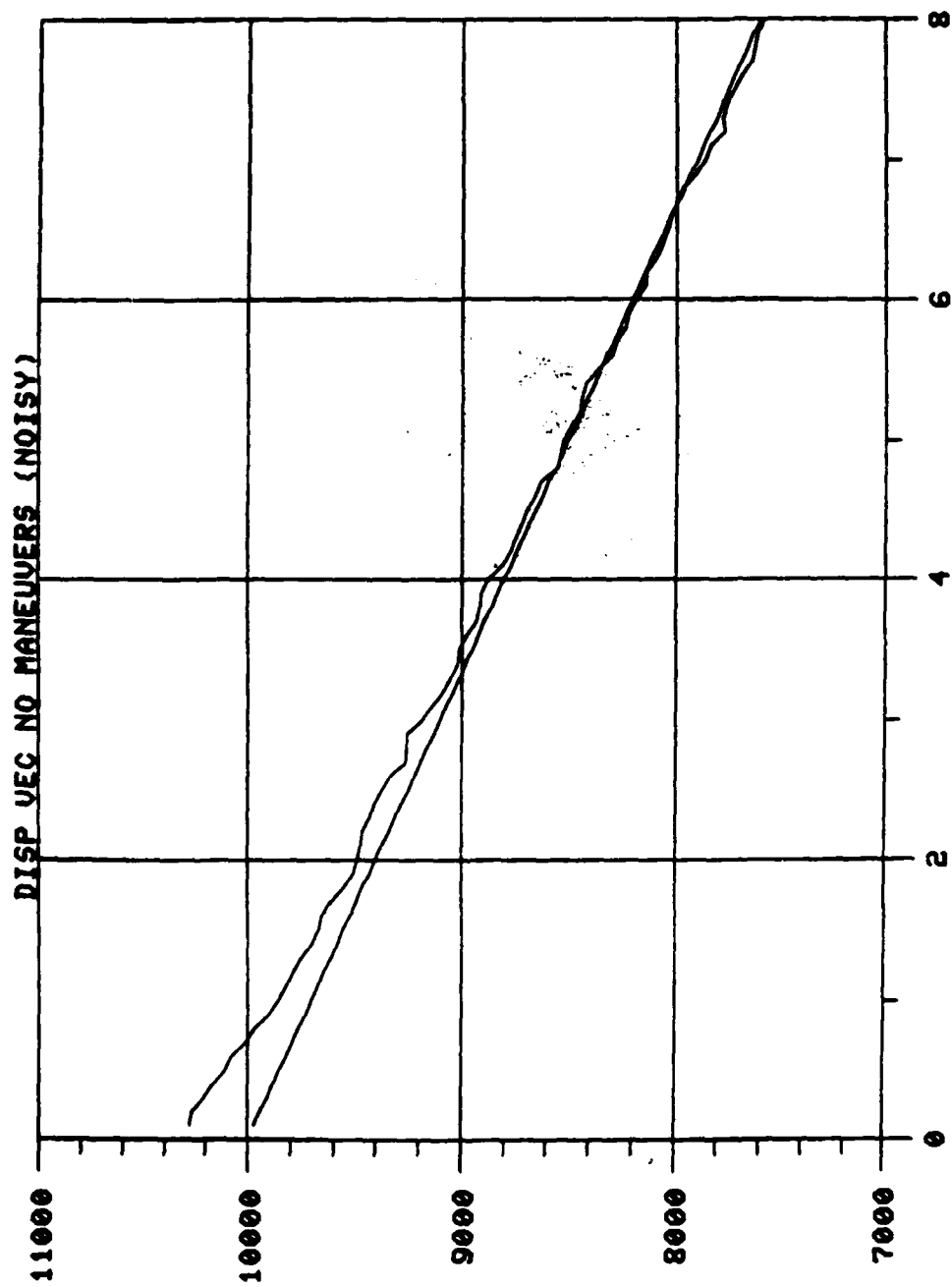


Figure 3

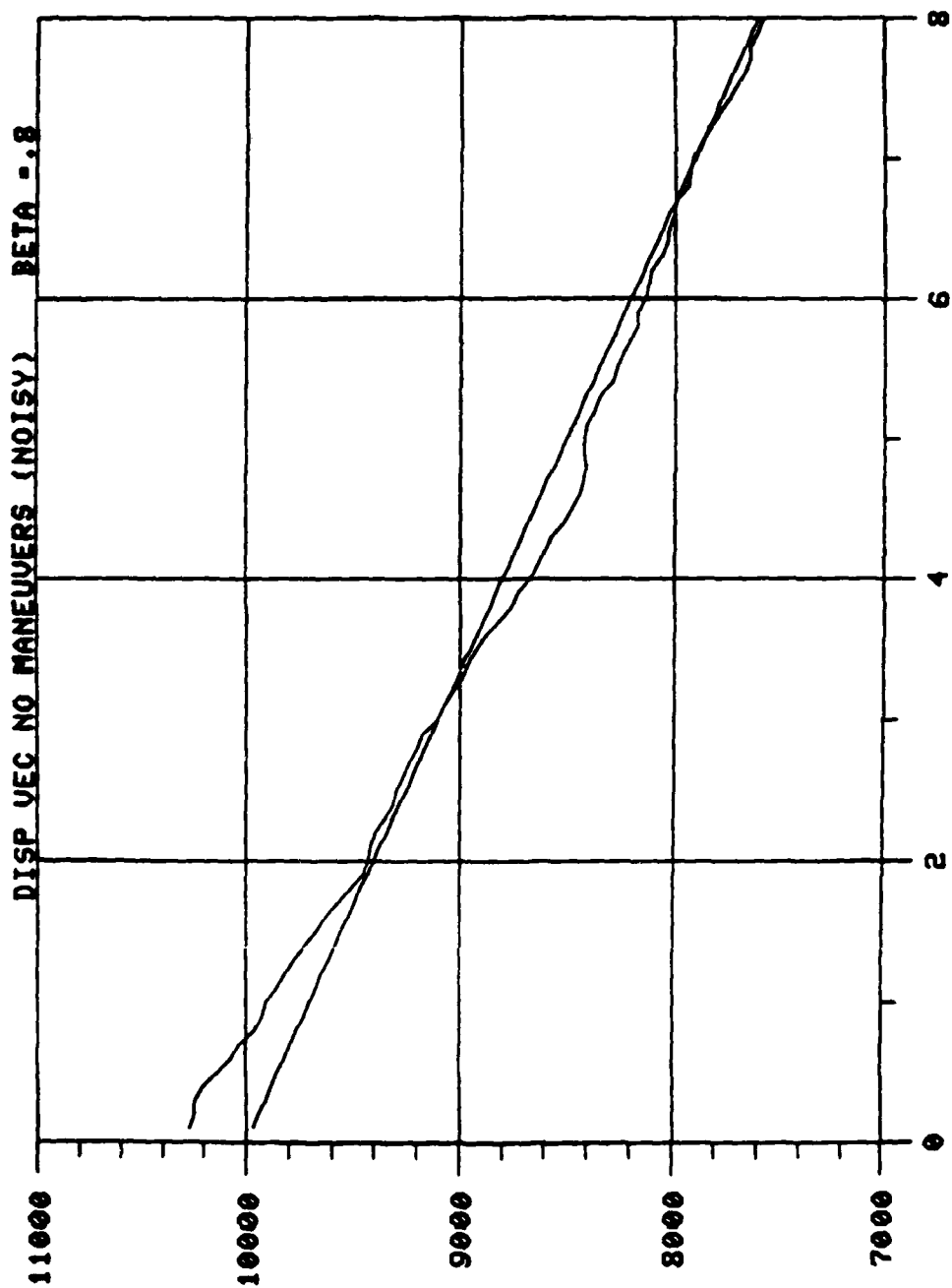


Figure 4

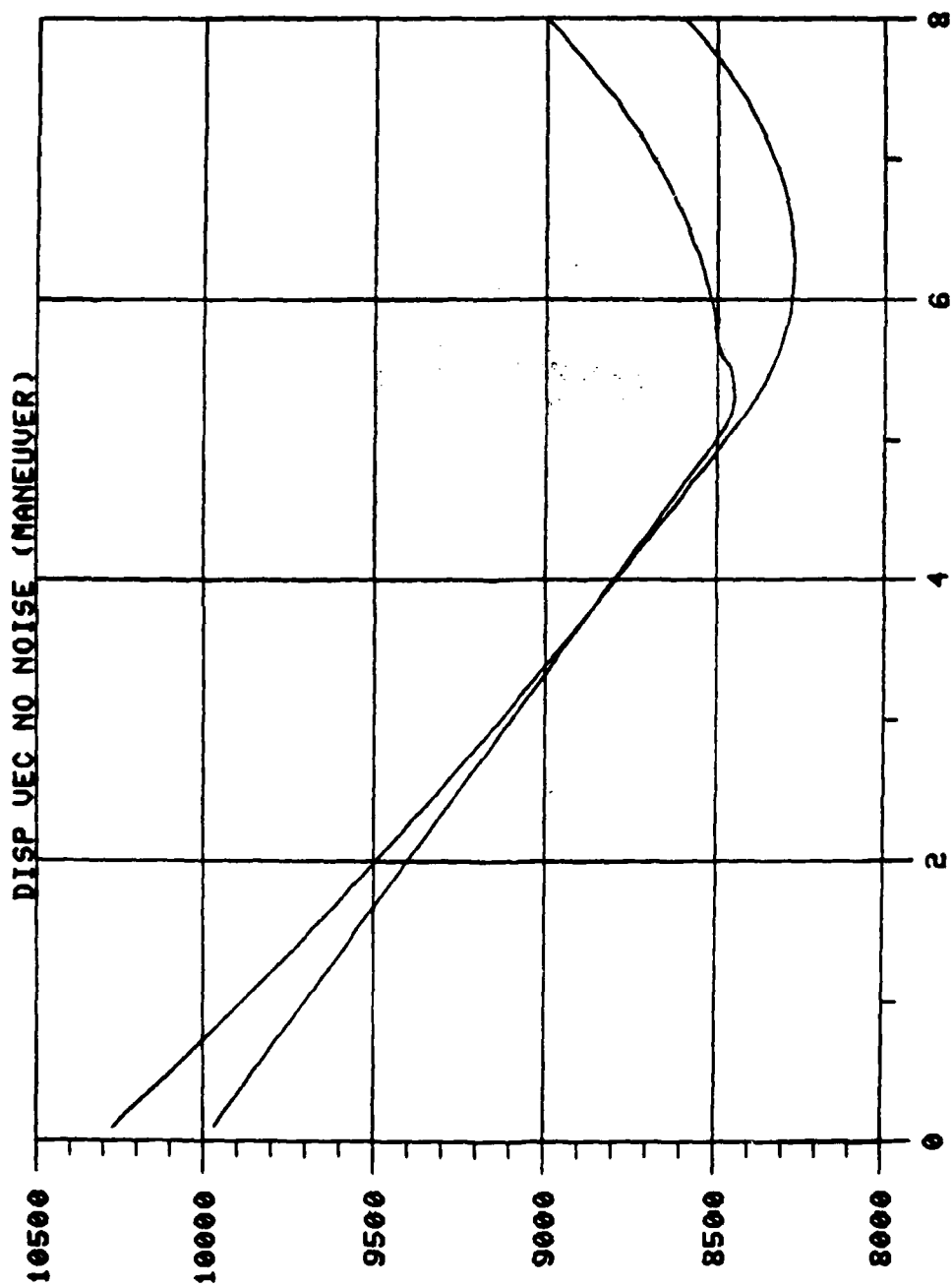


Figure 5



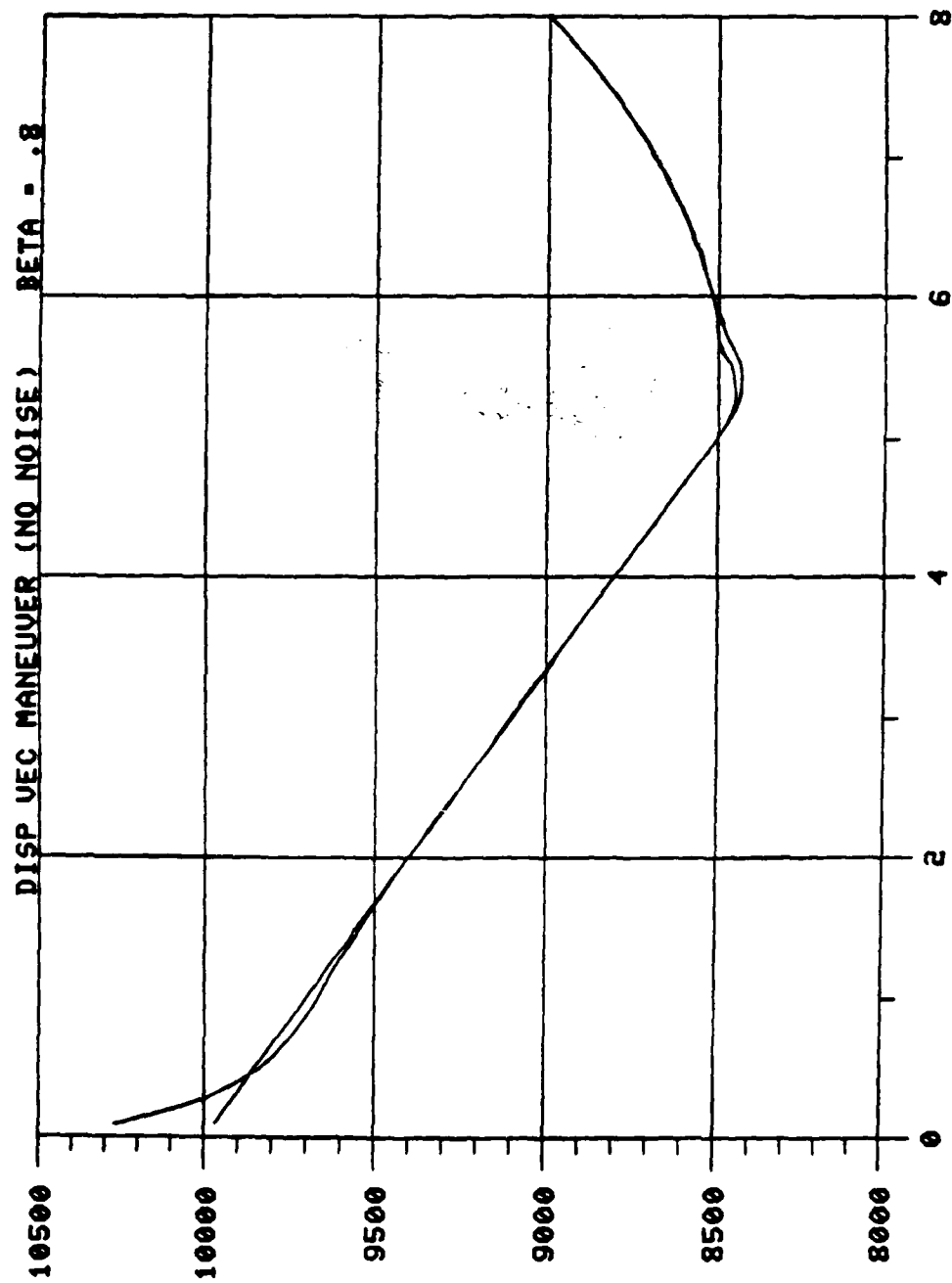


Figure 6

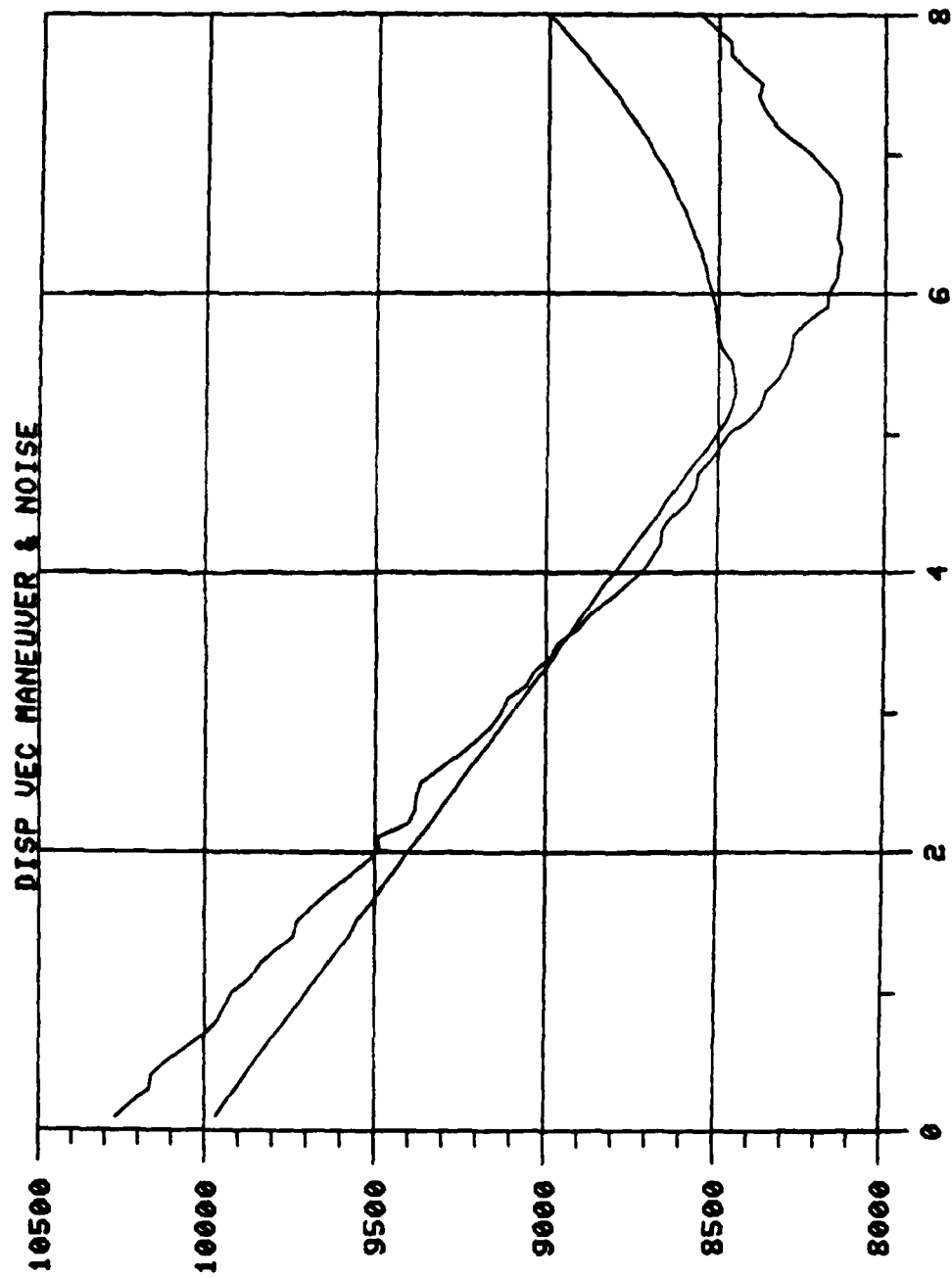


Figure 7

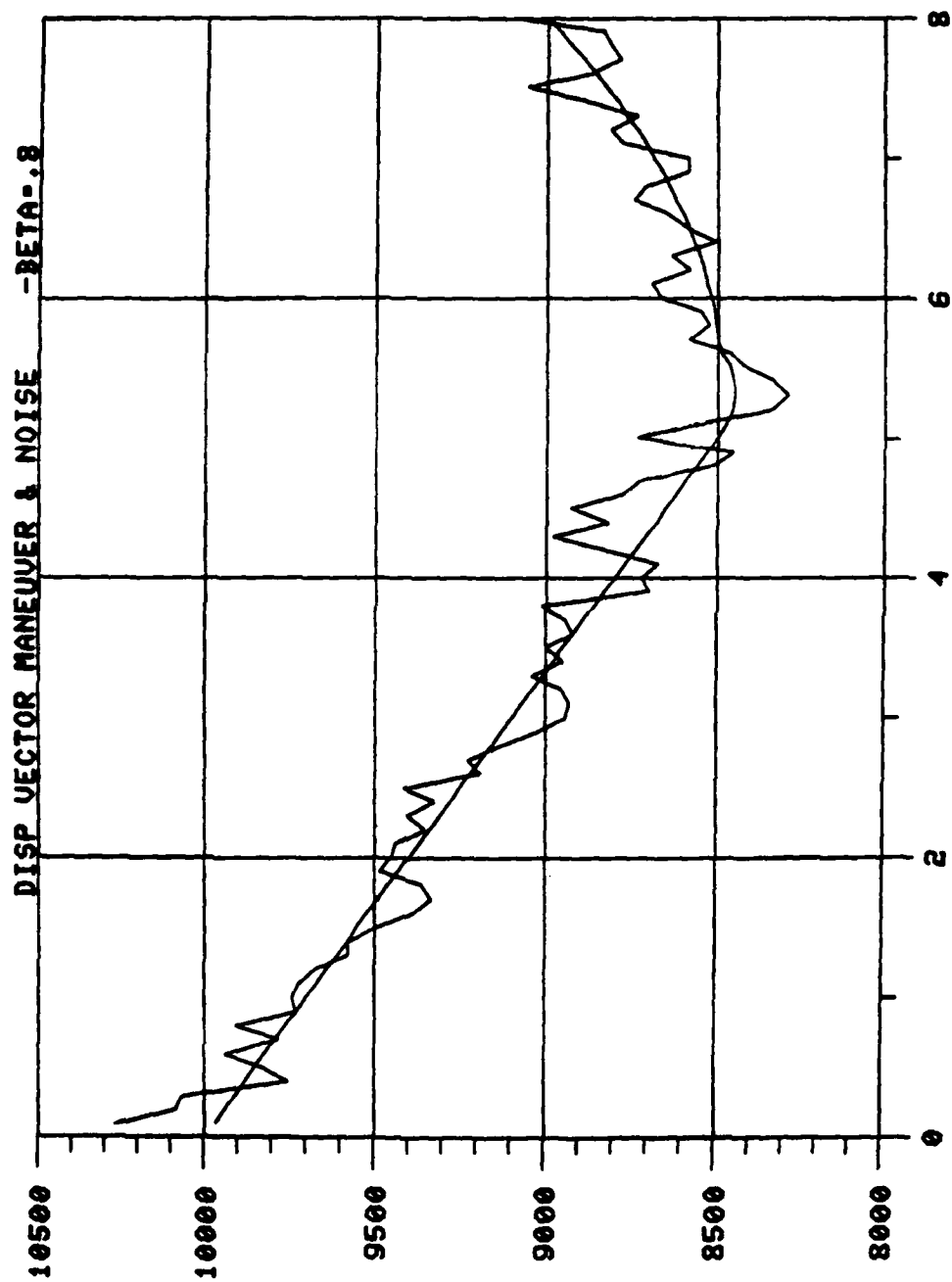


Figure 8

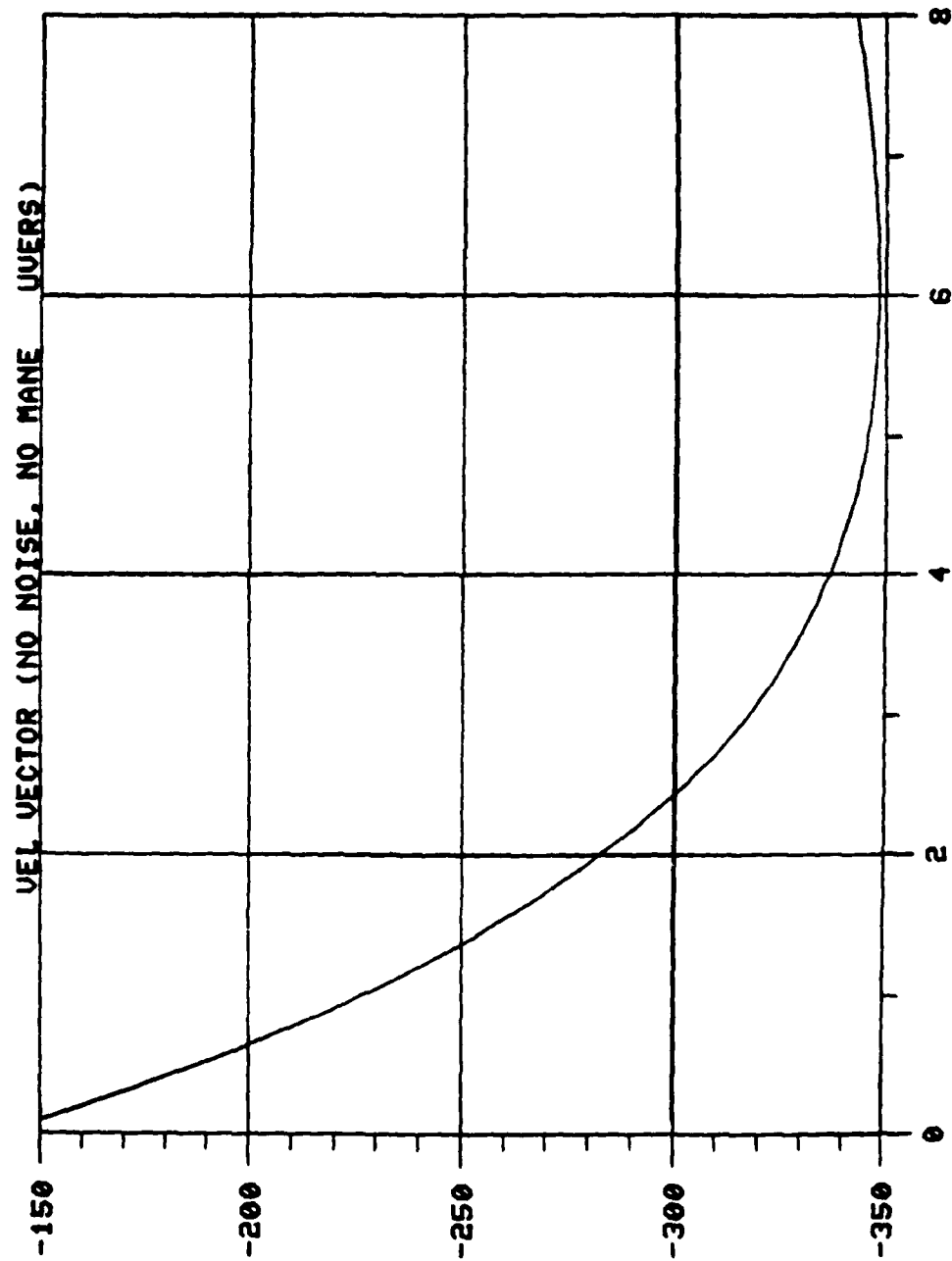


Figure 9

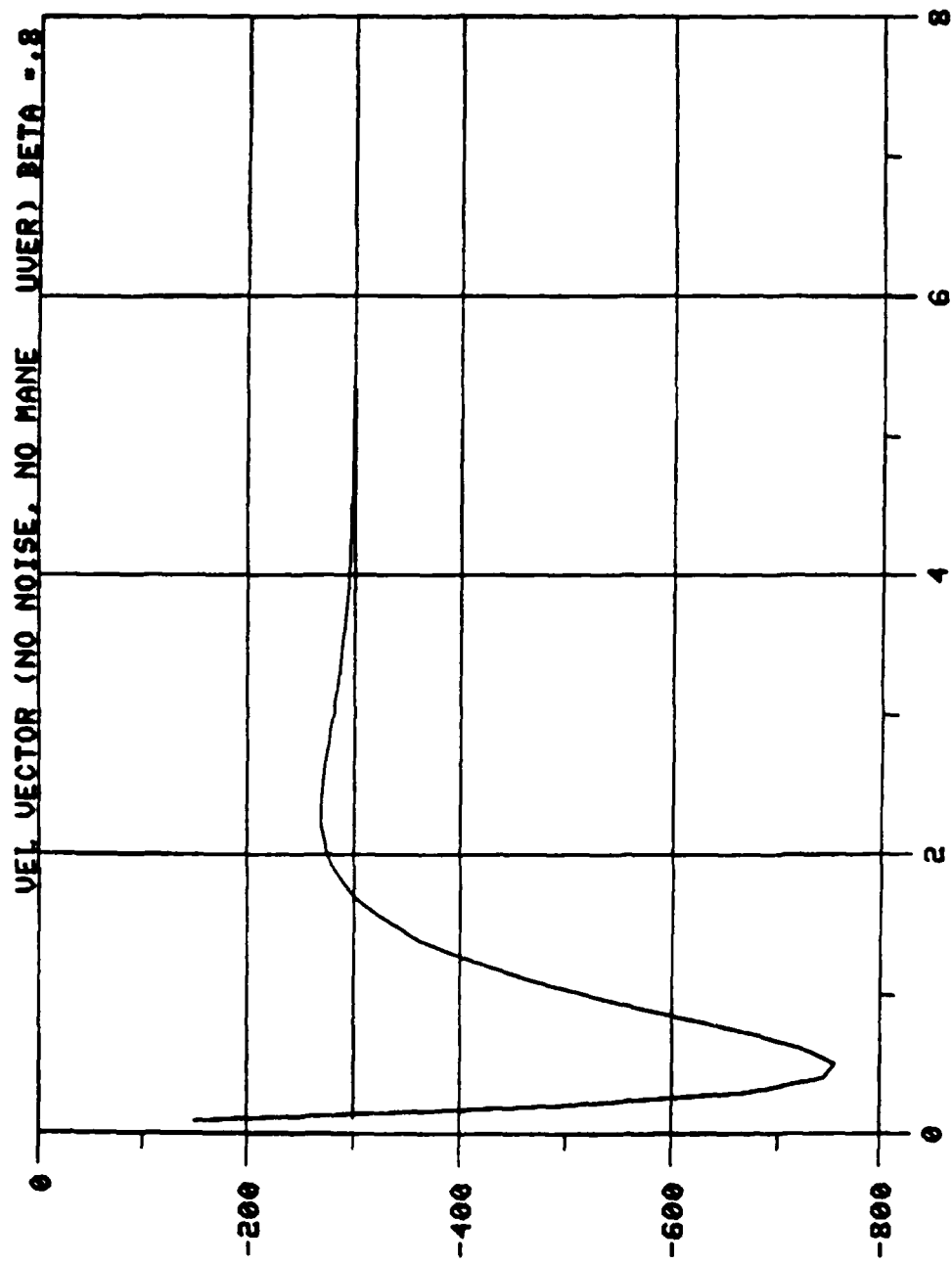


Figure 10

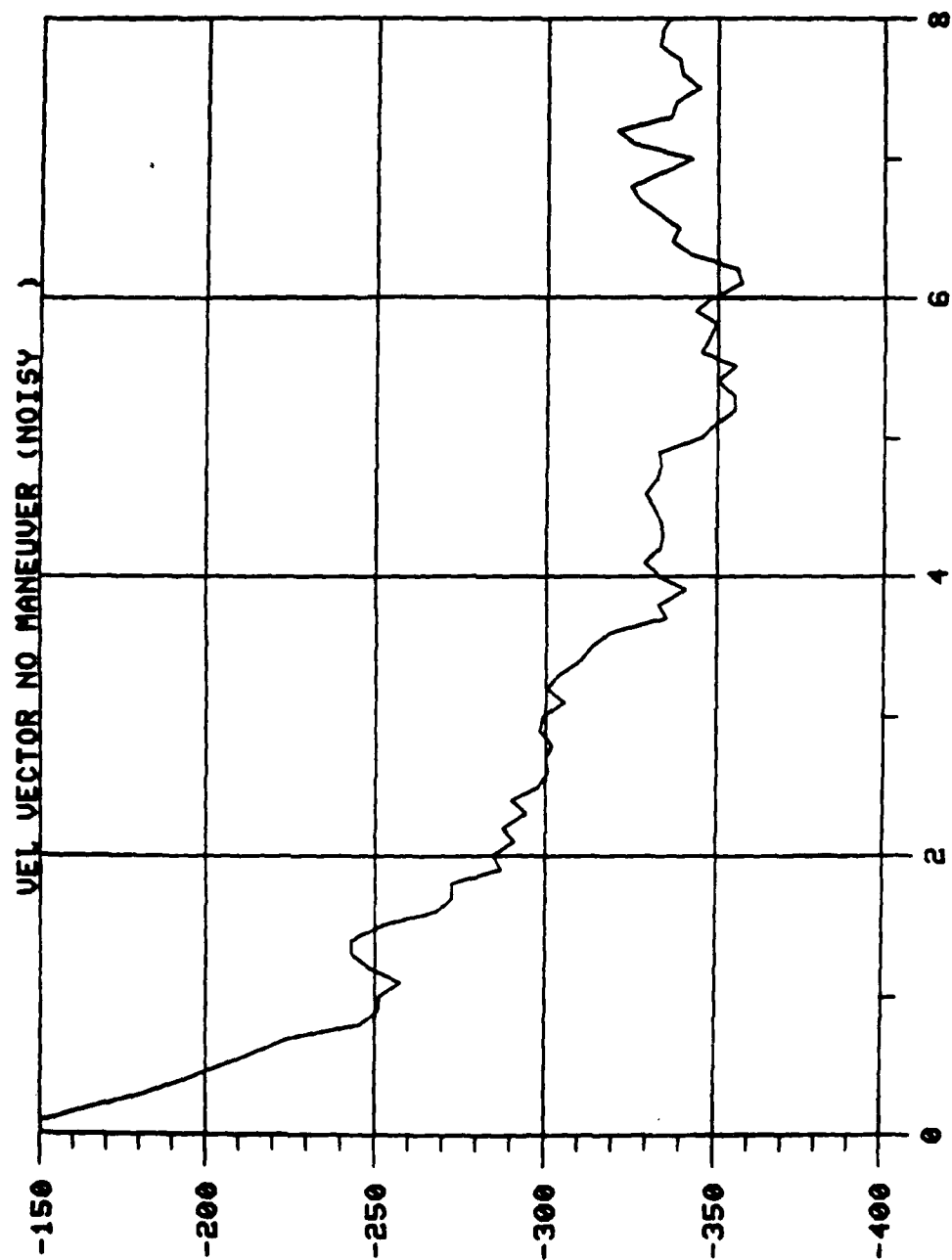


Figure 11

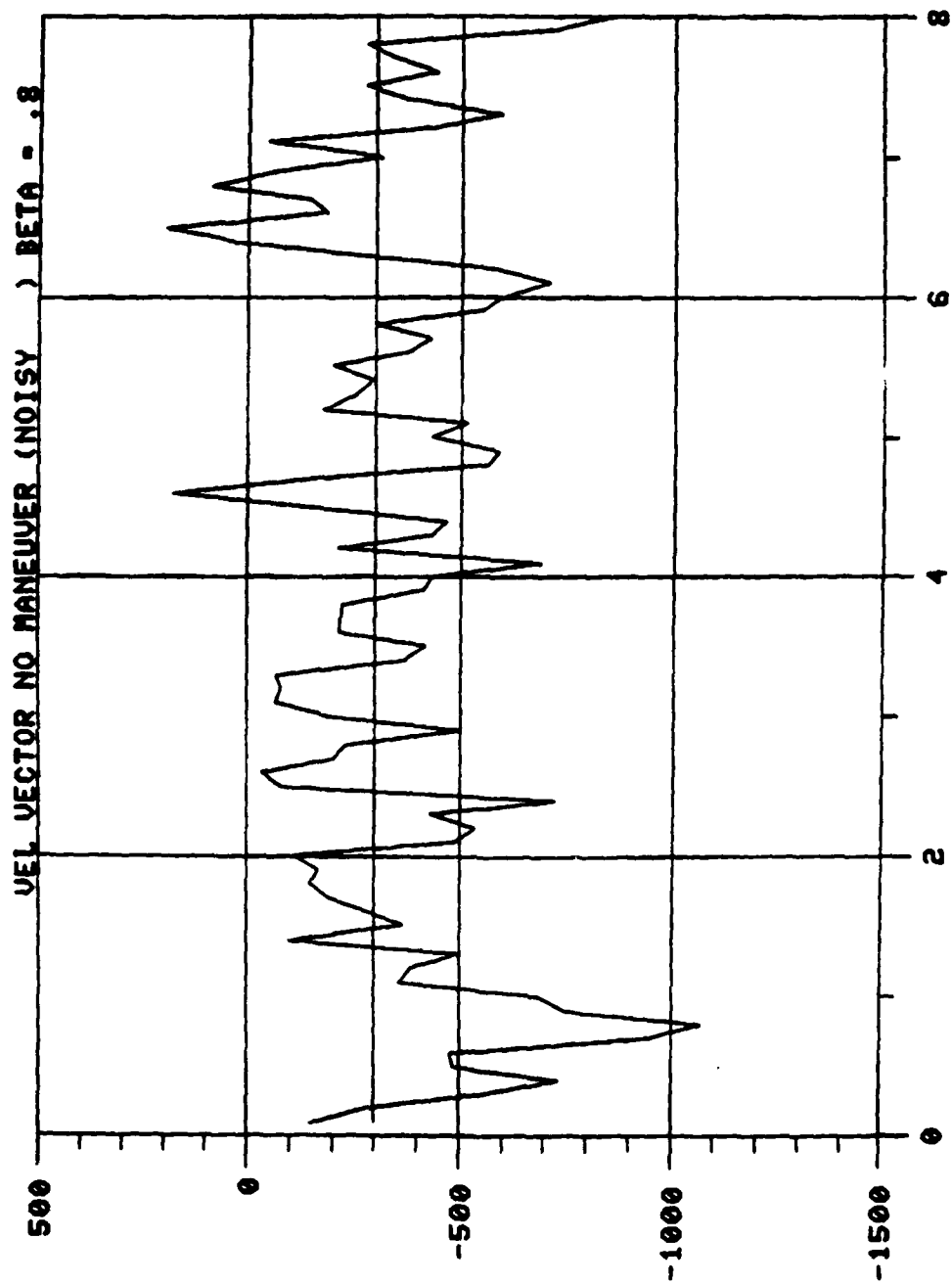


Figure 12

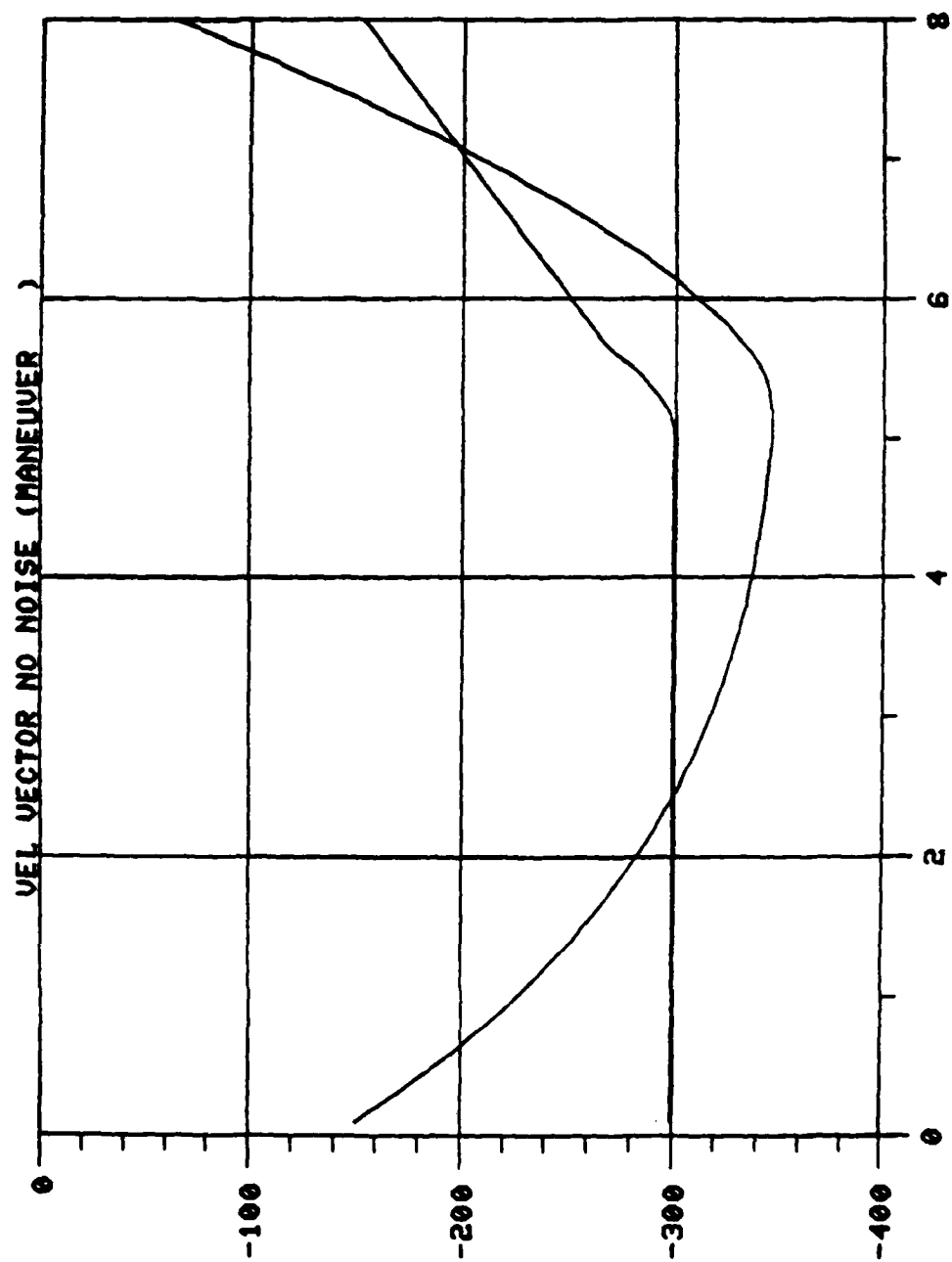


Figure 13



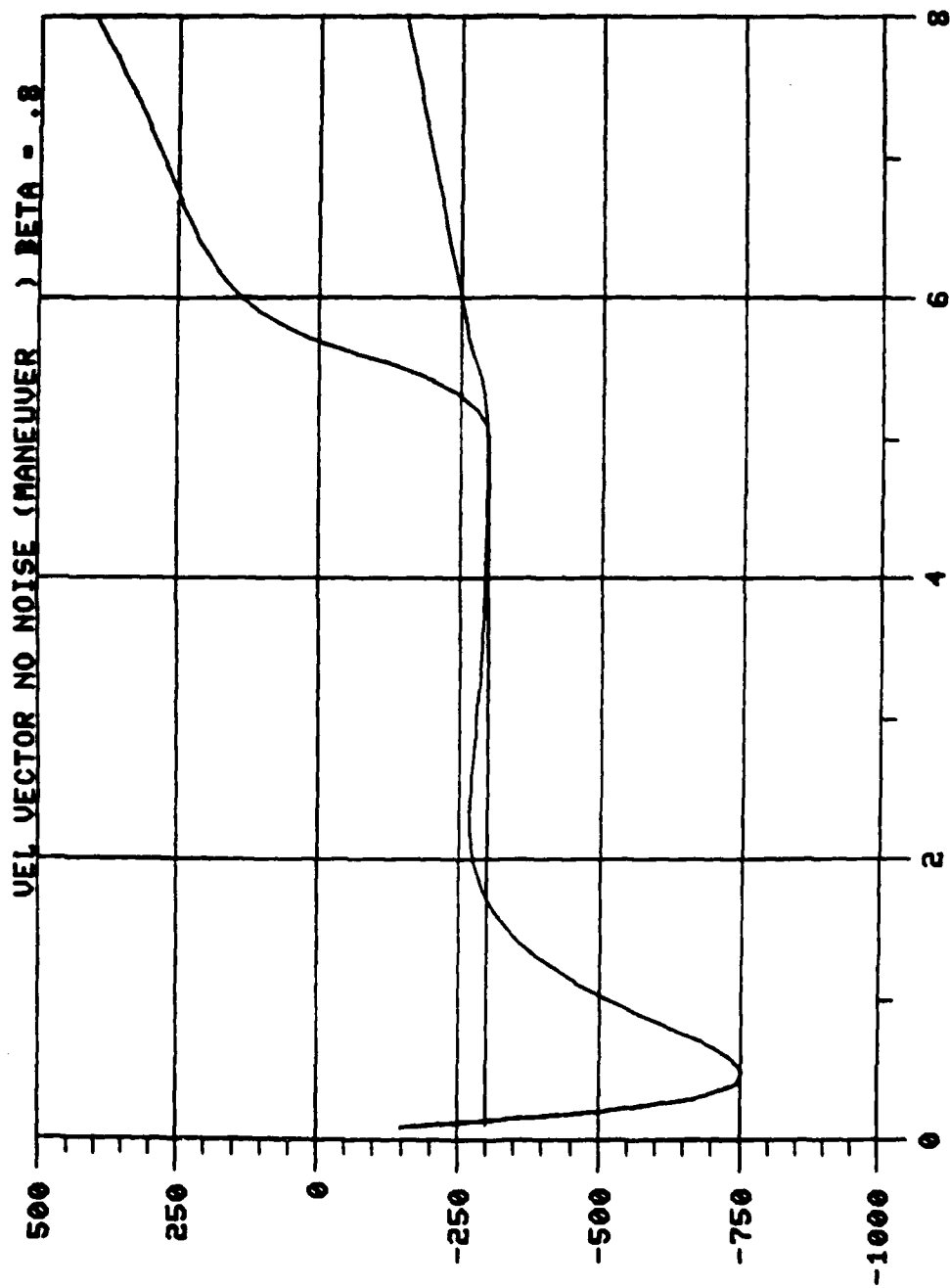


Figure 14

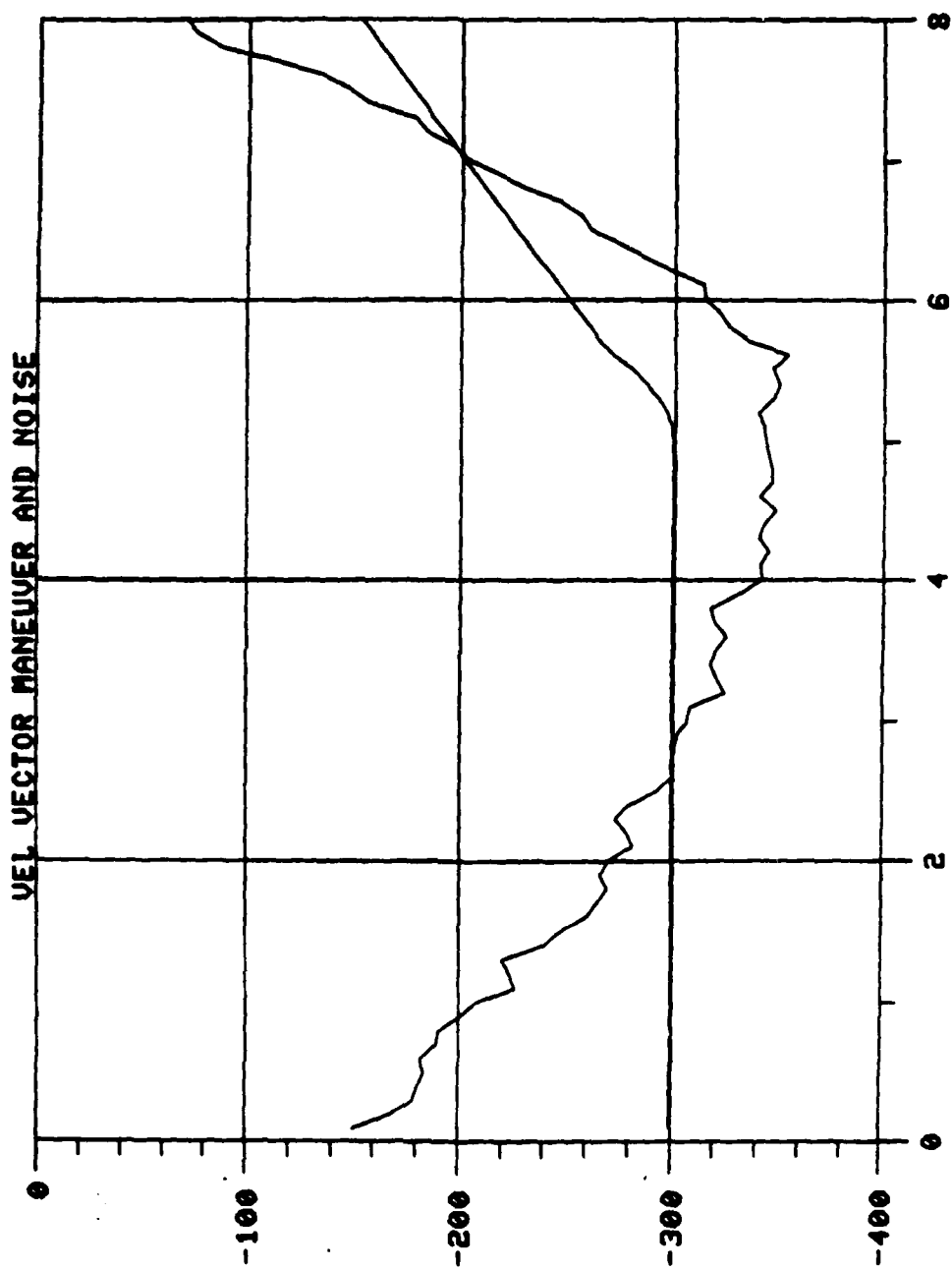


Figure 15

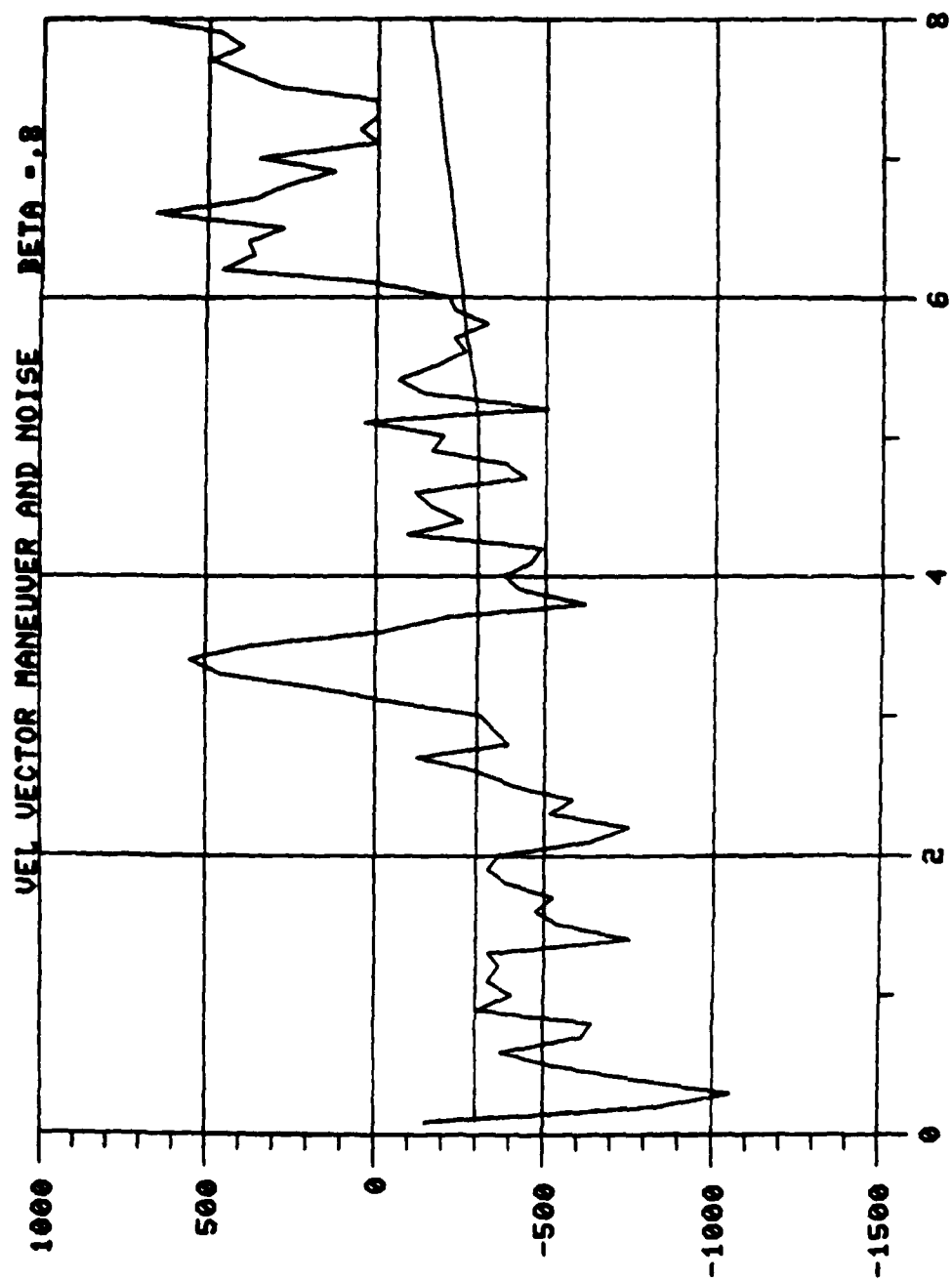


Figure 16

# MAIN PROGRAM

```

C      THIS IS A GRK ESTIMATOR
      DIMENSION ZH(100), XBA9H(100), ZOH(100), XDBA9H(100)
      DIMENSION ZOH(100), IT(100), ADL6H(100)
      CHARACTER *20 NAME
      REAL X,KV
      INTEGER C1
      R = (DELT**2)/2. =>
5      W = 0.
      C1 = 0
      NO = 1
C
10     FORMAT('1',3H,'INPUT SECTION')
20     FORMAT(1X,'*****')
1*****
C
C      TYPE 30
30     FORMAT('1','***** ALL VALUES ENTERED ARE FLOATING POINT -- UNLES
IS OTHERWISE INDICATED****')
35     TYPE 40
40     FORMAT(1X,'PLEASE ENTER NAME TO CALL THIS SET OF OUTPUT')
      READ(5,50) NAME
50     FORMAT(A1)
      PRINT 60, NAME
60     FORMAT(1X,'NAME OF OUTPUT IS ',A1)
C
C
70     TYPE 80
80     FORMAT(1X,'SEED MUST BE AN ODD INTEGER')
1     * PLEASE ENTER SEED NUMBER FOR SUBROUTINE
      READ(5,90,E9) NO
90     FORMAT(15)
      PRINT 100, NO
100    FORMAT(2X,'SEED NUMBER IS ',15/)
110    FORMAT(9X,'SEED FOR THIS RUN IS ',15/)
C CHECK TO SEE IF SEED IS WITHIN SPECIFIED BOUNDS
      IF(NO .LE. 1 .OR. NO .GT. 32768) THEN
          PRINT *, 'ERROR----- SEED MUST BE BETWEEN 1 AND 32768'
          GO TO 70
      ELSE
          CONTINUE
      ENDIF
C CHECK TO SEE IF SEED IS ODD
      NH1 = NO/2
      NH1 = NO/2.
      IF(NH1 .EQ. NH1) THEN
          PRINT *, '-----ERROR-----'
          GO TO 70
      ELSE
          CONTINUE
      ENDIF
      WRITE(6,10)
      WRITE(6,20)
      WRITE(6,60) NAME
      WRITE(6,110) NO
C
C
      IF (NH1.EQ.1) GO TO 175
      TYPE 120
120    FORMAT(1X,' XBA9=ESTIMATE OF POSITION',1X,' XDBA9 = TIME DERIVATI
IVE ESTIMATE',1X,' XDBA9=ESTIMATE OF ACCELERATION')

```



```

1 1X,'ZDD=ACCELERATION'/)
280 C1 = 1
290 TYPE 300
300 FORMAT(1X,'PLEASE ENTER Z1, ZD1, AND ZDD')
    READ(5,150,ERR=290) Z1, ZD1, ZDD
310 FORMAT(1X,' Z1=',E12.5,' ZD1=',E12.5,' ZDD=',E12.5/)
320 FORMAT(15X,' Z1=',E12.5,' ZD1=',E12.5,' ZDD=',F12.5/)
325 PRINT 310, Z1, ZD1, ZDD
    TYPE 190
    ACCEPT 200, C1
    IF(C1 .EQ. 1) GO TO 280
    WRITE (6,320) Z1, ZD1, ZDD

C
    Z1V = Z1
    ZD1V = ZD1
    ZDDV = ZDD

C
    IF(NR .EQ. 1) GO TO 415
    TYPE 330
330 FORMAT(1X,'T = TIME',/1X,'DELT = TIME INCREMENT',/1X,'TM = TIME OF
    MANEUVER'/)

C
C
    TYPE 340
340 FORMAT(1X,'IMAX=NUMBER OF COMPUTATIONAL STEPS'/)
    TYPE 350
    C1 = 0
360 FORMAT(1X,'PLEASE ENTER T, DELT, TM, AND IMAX (INTEGER)')
    READ(5,370,ERR=350) T, DELT, TM, IMAX
370 FORMAT(3F6.2,I3)
380 FORMAT(1X,'IMAX=',I3/)
390 FORMAT(16X,'IMAX=',I3/)
400 FORMAT(1X,' T= ',F6.2,' DELT= ',F6.2,' TM= ',F6.2/)
410 FORMAT(15X,' T= ',F6.2,' DELT= ',F6.2,' TM= ',F6.2/)
415 PRINT 380, IMAX
    PRINT 400, T, DELT, TM
    TYPE 190
    ACCEPT 200, C1
    IF(C1 .EQ. 1) GO TO 350
    WRITE (6,390) IMAX
    WRITE (6,410) T, DELT, TM
    WRITE(6,20)
C HOLD VALUES OF T, DELT, TM, AND IMAX
    TV = T
    TMV = TM
    DELTV = DELT
    IMAXV = IMAX

C
    WRITE(6,420)
420 FORMAT('1')
C
C ***** COMPUTATION SECTION *****
430 TYPE 430
    C1 = 0
435 FORMAT (1X,' ENTER 1 TO PRINT RESULTS FOR EACH STEP ')
    READ(5,200,ERR=430) C1

C
    CALL GAUSS (NO,SIG,PMEAN,NG)

    DO 140 I=1,IMAX
        T = T + DELT

```

```

C
C      STORE VALUES TO BE PRINTED, TO AN ARRAY
C
      ZH(I)      = Z
      XBARH(I)   = XBAR
      ZDH(I)     = ZD
      XDBARH(I)  = XDBAR
      ZDDH(I)    = ZDD
      XDDH(I)    = XDDBAR
      TT(I)      = T

C
440    CONTINUE
C
C      ***** PRINT VALUES STORED IN ARRAY *****
      WRITE(6, 590)
590    FORMAT('1', 'STEP', 4X, 'Z', 1X, 'XBAR', 1X, 'ZD', 1X, 'XDBAR',
1      AX, 'ZDD', 1X, 'XDDBAR'//)
C
      DO 591 JP = 1, IMAX
      *RITE(6, 600) JP, ZH(JP), XBARH(JP), ZDH(JP), XDBARH(JP),
1      ZDDH(JP), XDDH(JP)
600    FORMAT(1X, I3, 6(1X, E12.5)//)
591    CONTINUE
C
C      CHECK TO SEE WHETHER PLOTS ARE WANTED
      C1 = 1
      PRINT *, 'ENTER 1 TO PLOT DATA'
      ACCEPT 200, C1
      IF (C1 .EQ. 1) THEN
C      CALL PLOT PROGRAM
C      CHECK TO SEE WHETHER TO PLOT DISPLACEMENT OR VELOCITY PLOTS
603      TYPE 605
605      FORMAT (' ENTER 1 TO PLOT DISPLACEMENT VECTOR//
1' ENTER 2 TO PLOT VELOCITY VECTOR//,
1' ENTER 3 TO PLOT ACCELERATION VECTOR//)
      C1 = 1
      ACCEPT 200, C1
      IF (C1 .NE. 1 .AND. C1 .NE. 2 .AND. C1 .NE. 3) THEN
        PRINT *, 'PLEASE ENTER 1 OR 2 OR 3'
        GO TO 603
      ELSE
        CONTINUE
      ENDIF
      IF (C1 .EQ. 1) CALL PEST (TT, XBARH, ZH, IMAX, 1, 6)
      IF (C1 .EQ. 2) CALL PEST (TT, XBARH, ZDH, IMAX, 1, 6)
      IF (C1 .EQ. 3) CALL PEST (TT, ZDDH, XDDH, IMAX, 1, 6)
C      END OF PLOT ROUTINE
      ELSE
        CONTINUE
      ENDIF
C
      PRINT 610, NAME
      WRITE(6, 610) NAME
610    FORMAT(1X, 'END OF JOB FOR PROGRAM ', 4A1)
C
C      CHECK FOR ANOTHER RUN
      TYPE 620
      NM = 0
620    FORMAT (' ENTER 1 TO MAKE ANOTHER RUN. ')
      ACCEPT 200, NM
      IF (NM .EQ. 1) THEN

```

```

      IF (NR .EQ. 1) THEN
C REINITIALIZE NAMES TO ORIGINAL VALUES
        XBAR = XEV
        XDBAR = XDBV
        XDDBAR = XDDBV
        SIG = SIGV
        RMEAN = RMNV
        Z1 = Z1V
        ZD1 = ZD1V
        ZDD = ZDDV
        S = SV
        G = GV
        H = HV
        K = KV
        T = TV
        TM = TMV
        DELT = DELV
        ZMAX = ZMAXV
        GO TO 5
      ELSE
        CONTINUE
      ENDIF
C
      STOP
      END

```



#### REFERENCES

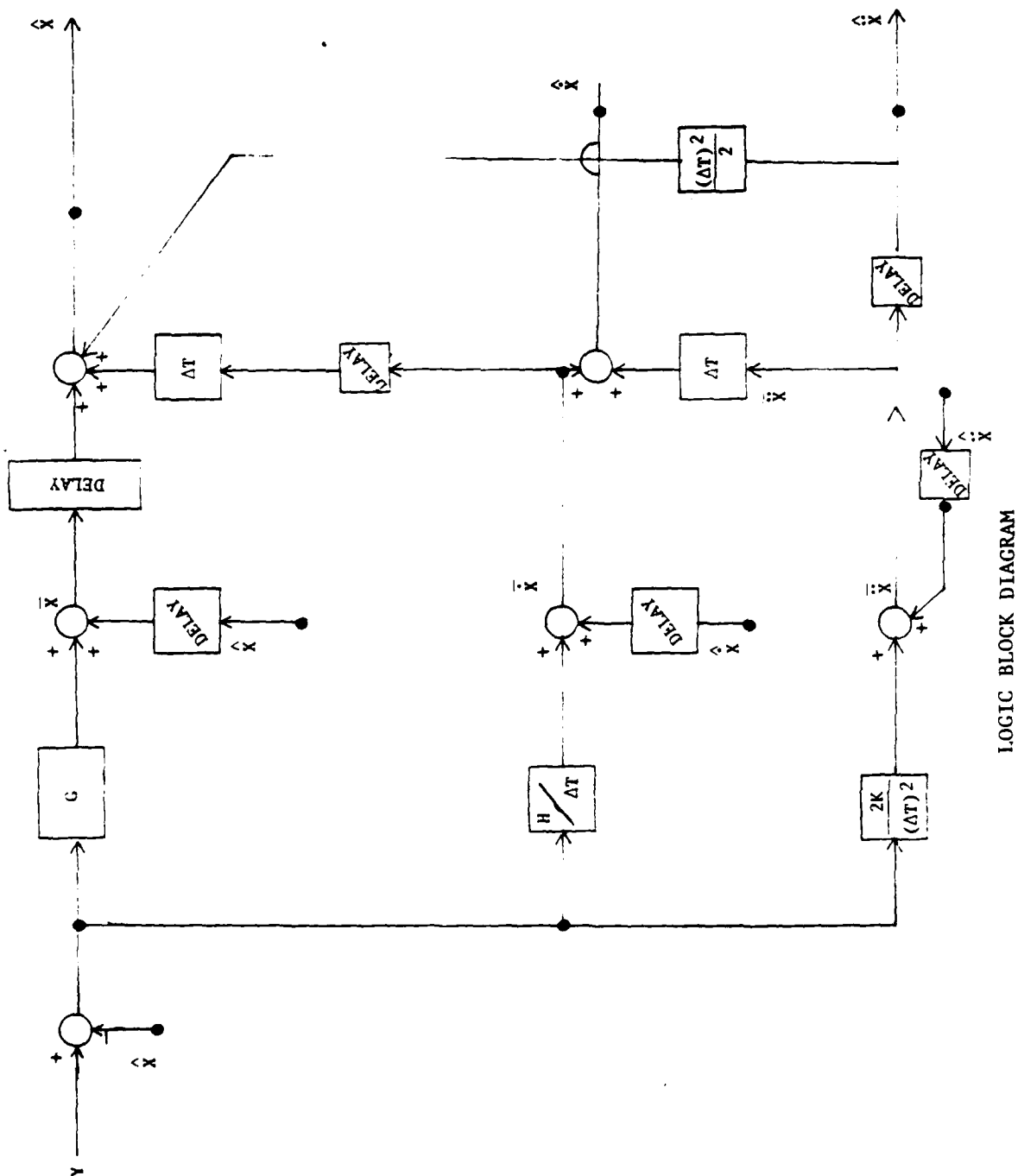
1. "Bistatic Tracking and Trajectory, Estimating Techniques," Henry C. Holman, Dissertation, Southeastern Institute of Technology, 1981.
2. "VAX 11/780" User's Guide.

## APPENDIX A

### OPERATING PROCEDURES

1. Procedure for running program:
  - a. LOG ON TO VAX 780
  - b. TYPE "ASSIGN EST.OUT FOR 006"
  - c. TYPE "ASSIGN EST.TEX FOR001"
  - d. TYPE "RUN EST"
  - e. FOLLOW PROMPTS
2. Procedure for obtaining hardcopies:
  - a. TYPE "PR EST.OUT"
  - b. OBTAIN HARDCOPY FROM OPERATOR
  - c. LOGIN ON TEKTRONIX NUMBER
  - d. TYPE "EST TEX"
  - e. PROGRAM SUPPORT CONTACT - SANDRA BRAZELTON/876-2295

APPENDIX B  
LOGIC BLOCK DIAGRAM



LOGIC BLOCK DIAGRAM

APPENDIX C  
SOURCE LISTING

```

C      MAIN PROGRAM
C      THIS IS A GMM ESTIMATOR
      DIMENSION ZH(100), XBARH(100), ZDH(100), XDAPH(100)
      DIMENSION ZDDH(100), ET(100), XDDSH(100)
      CHARACTER *20 NAME
      REAL K,KV
      INTEGER C1
5      N = 0.
      C1 = C
      NO = 1

C
10     FORMAT('1',30X,'INPUT SECTION')
20     FORMAT(1X,'*****')
1 *****'
C
C      TYPE 30
30     FORMAT('1','***** ALL VALUES ENTERED ARE FLOATING POINT --UNLES
1S OTHERWISE INDICATED****'//)
35     TYPE 40
40     FORMAT(1X,'PLEASE ENTER NAME TO CALL THIS SET OF OUTPUT')
      READ(5,50) NAME
50     FORMAT(A60)
      PRINT 60, NAME
60     FORMAT(10X,'NAME OF OUTPUT IS ',A60)
C
C
70     TYPE 30
80     FORMAT(1X,'SEED MUST BE AN ODD INTEGER '//,
1 ' PLEASE ENTER SEED NUMBER FOR SUBROUTINE')
      READ(5,90,ERR = 70) NO
90     FORMAT(I5)
      PRINT 100, NO
100    FORMAT(2X,'SEED NUMBER IS ',I5/)
110    FORMAT(2X,'SEED FOR THIS RUN IS ',I5//)
C CHECK TO SEE IF SEED IS WITHIN SPECIFIED BOUNDS
      IF(NO .LE. 0 .OR. NO .GT. 32768) THEN
          PRINT *, 'ERROR----- SEED MUST BE BETWEEN 0 AND 32768'
          GO TO 70
      ELSE
          CONTINUE
      ENDIF
C CHECK TO SEE IF SEED IS ODD
      NM1 = NO/2
      NM1 = NO/2.
      IF(NM1 .EQ. NM1) THEN
          PRINT *, '---ERROR---'
          GO TO 70
      ELSE
          CONTINUE
      ENDIF
      WRITE(6,10)
      WRITE(6,20)
      WRITE(6,60) NAME
      WRITE(6,110) NO

C
C
      IF (NM1.EQ.1) GO TO 175
      TYPE 120
120    FORMAT(1X,' XBAR=ESTIMATE OF POSITION',1X,' XDEAR = TIME DERIVAT
1VE ESTIMATE',1X,' XDDBAR=ESTIMATE OF ACCELERATION')

```

```

C
130 TYPE 140
140 FORMAT(1X,'PLEASE ENTER XBAR,XDBAR, AND XDDBAR')
    C1 = C
    READ(5,150,ERR=130) XBAR, XDBAR, XDDBAR
150 FORMAT(F5.2,2(E12.5))
160 FORMAT(1X,'XBAR= ',F5.2,' XDBAR= ',E12.5,' XDDBAR= ',E12.5/)
170 FORMAT(14X,'XBAR= ',F5.2,' XDBAR= ',E12.5,' XDDBAR= ',
1 E12.5/)
175 TYPE 160, XBAR, XDBAR, XDDBAR
180 TYPE 190
190 FORMAT(1X,'ENTER 1 TO CHANGE VALUES JUST ENTERED')
    ACCEPT 200, C1
200 FORMAT(I1)
    IF(C1 .EQ. 1) GO TO 130
    WRITE (6,170) XBAR, XDBAR, XDDBAR

C
C    HOLD VALUES
XBV = XBAR
XDBV = XDBAR
XDDBV = XDDBAR

C
    IF (NR .EQ. 1) THEN
        PRINT 210, G, H, K
        PRINT 215, B
215 FORMAT(2X,'BETA IS ',E16.9/)
210 FORMAT(16X,'G= ',E14.7,' H= ',E14.7,' K= ',E14.7/)
        PRINT *, 'ENTER 1 TO CHANGE BETA'
        ACCEPT 200, C1
        IF(C1 .EQ. 1) CALL GHK(G, H, K, B)
        CONTINUE
    ELSE
        CALL GHK (G, H, K, B)
        WRITE (6,210) G, H, K
    ENDIF
C    HOLD VALUE OF BETA G, H, AND K
    GV = G
    HV = H
    KV = K
    BV = B

C
    IF (NR .EQ. 1) GO TO 255
220 TYPE 230
    C1 = C
230 FORMAT(1X,'ENTER GAUSSIAN NOISE SIGMA AND NOISE MEAN')
    READ (5,240,ERR=220) SIG, RMEAN
240 FORMAT(1X,'NOISE FACTOR IS ',F5.2,' MEAN IS ',F5.2/)
250 FORMAT(1X,'NOISE FACTOR IS ',F5.2,' MEAN IS ',F5.2/)
255 PRINT 240, SIG, RMEAN
260 FORMAT(F5.2)
    TYPE 170
    ACCEPT 200, C1
    IF(C1 .EQ. 1) GO TO 220
    WRITE (6,250) SIG, RMEAN

C
    SIGV = SIG
    RMNV = RMEAN

C
    IF(NR .EQ. 1) GO TO 325
    TYPE 270
270 FORMAT(1X,'Z1=INITIAL TRUE POSITION',1X,'ZD1=TIME DERIVATIVE',/

```

```

1 1X,'ZDD=ACCELERATION'//)
280 C1 = 0
290 TYPE 300
300 FORMAT(1X,'PLEASE ENTER Z1, ZD1, AND ZDD')
    READ(5,130,ERR=290) Z1, ZD1, ZDD
310 FORMAT(1X,' Z1=',E12.5,' ZD1=',E12.5,' ZDD=',E12.5//)
320 FORMAT(15X,' Z1=',E12.5,' ZD1=',E12.5,' ZDD=',E12.5//)
325 PRINT 310, Z1, ZD1, ZDD
    TYPE 190
    ACCEPT 200, C1
    IF(C1 .EQ. 1) GO TO 230
    WRITE (6,320) Z1, ZD1, ZDD

C
    Z1V = Z1
    ZD1V = ZD1
    ZDDV = ZDD

C
    IF(NR .EQ. 1) GO TO 415
    TYPE 330
330 FORMAT(1X,'T = TIME',/1X,'DELT = TIME INCREMENT',/1X,'TM = TIME C
    1,MANEUVER'//)

C
C
    TYPE 340
340 FORMAT(1X,'IMAX=NUMBER OF COMPUTATIONAL STEPS'//)
350 TYPE 350
    C1 = 0
360 FORMAT(1X,'PLEASE ENTER T, DELT, TM, AND IMAX (INTEGER)')
    READ(5,370,ERR=350) T, DELT, TM, IMAX
370 FORMAT(3F6.2,I3//)
380 FORMAT(1X,'IMAX= ',I3//)
390 FORMAT(16X,'IMAX= ',I3//)
400 FORMAT(1X,' T= ',F6.2,' DELT= ',F6.2,' TM= ',F6.2//)
410 FORMAT(15X,' T= ',F6.2,' DELT= ',F6.2,' TM= ',F6.2//)
415 PRINT 380, IMAX
    PRINT 400, T, DELT, TM
    TYPE 190
    ACCEPT 200, C1
    IF(C1 .EQ. 1) GO TO 350
    WRITE (6,390) IMAX
    WRITE (6,410) T, DELT, TM
    WRITE(6,20)

C HOLD VALUES OF T, DELT, TM, AND IMAX
    TV = T
    TMV = TM
    DELV = DELT
    IMAXV = IMAX

C
    WRITE(6,420)
420 FORMAT('1')

C
C ***** COMPUTATION SECTION *****
430 TYPE 430
    C1 = 0
435 FORMAT (1X,' ENTER 1 TO PRINT RESULTS FOR EACH STEP ')
    READ(5,200,ERR=430) C1

C
    DO 440 I=1,IMAX
    T = T + DELT
    IF (T .LT. TM) GO TO 450

```



```

      ZDD = 79.5 * (T-TM)
      IF (ZDD .GE. 49.1) ZDD = 49.1
450    ZD = ZD1 + ZDD * (T-TM)
      Z = Z1 + ZD*T
      IF (T .GE. TM) Z = Z + 0.5 * ZDD * (T-TM)**2

C
      CALL GAUSS (NC,SIG,PMEAN,WG)
      Y = Z + WG

C
C
      IF (I .EQ. 1) GO TO 460
C***** ESTIMATE AT CURRENT TIME *****
C*****
C      NEXT THREE STATEMENTS ARE SKIPPED ON FIRST PASS
C*****
      XBAR = XHAT + G * (Y-XHAT)
      XDBAR = XDBAT + (H/DELT) * (Y-XHAT)
      XDDBAR = XDDBAT + ((2 * K)/(DELT**2)) * (Y-XHAT)
C*****
C      THIS IS THE LOGIC FOR THE FIRST PASS
C*****
C
      R = (DELT**2)/2.
460    XHAT = XBAR + XDBAR * DELT + XDDBAR * R
      XDBAT = XDBAR + XDDBAR * DELT
      XDDBAT = XDDBAR

C
C***** PRINT ROUTINE *****
C
C      **** CHECK TO SEE IF ALL RESULTS ARE TO BE PRINTED ***
C
      IF (C1 .EQ. 0) GO TO 470
C
C      **** SKIP THIS SECTION IF C1 = 0 *****
C
      WRITE (6, 430)Z
430    FORMAT(1JX,'RESULTS FOR STEP ',I3/)
      WRITE (6, 490)
490    FORMAT(3X,'T',I3X,' XBAR ',9X,' XDBAR ',5X,' XDDBAR')
      WRITE (6, 500)T, XBAR, XDBAR, XDDBAR
500    FORMAT(1A,E12.5,1X,E12.5,2X,E12.5,1X,E12.5//)
      WRITE (6, 510)
510    FORMAT(3X,' XHAT ',9X,' XDBAT ',3X,' XDDBAT')
      WRITE (6, 520) XHAT, XDBAT, XDDBAT
520    FORMAT(3X,3(E12.5,3X)//)
      WRITE (6, 530)
530    FORMAT(5X,'Z ',15X,'ZD ',14X,'ZDD')
      WRITE (6, 540) Z, ZD, ZDD
540    FORMAT(4X,E12.5,4X,E12.5,4X,E12.5//)
      WRITE (6, 550)
550    FORMAT(3X,'XBAR = Z ',9X,'XDBAR-ZD ',7X,'XDDBAR-ZDD')
      WRITE (6, 560) (XBAR-ZD), (XDBAR-ZD), (XDDBAR-ZDD)
560    FORMAT(3X,3(E12.5,3X)//)
      WRITE (6, 570) Y, (Y-XHAT)
570    FORMAT(1X,'Y= ',E12.5,3X,'(Y-XHAT) = ',E12.5//)
C
C ***** END OF SECTION TO BE SKIPPED *****
C
C

```

```

470 CONTINUE!C1 = 0 DO ONLY PRINT VALUES STORED IN ARRAY
C
C STOPE VALUES TO BE PRINTED IN AN ARRAY
C
      ZH(I) = Z
      XBARM(I) = XBAR
      ZDH(I) = ZD
      XDARM(I) = XDBAR
      ZDDH(I) = ZDD
      XDDSH(I) = XDDBAR
      TT(I) = T
C
440 CONTINUE
C
C ***** PRINT VALUES STORED IN ARRAY *****
      WRITE(6, 530)
580 FORMAT('1', 'STEP', 4X, 'Z', 10X, 'XBAR', 10X, 'ZD', 10X, 'XDBAR',
1 2X, 'ZDD', 10X, 'XDDBAR'//)
C
      DO 590 JP = 1, IMAX
      WRITE(6, 400) JP, ZH(JP), XBARM(JP), ZDH(JP), XDARM(JP),
1 ZDDH(JP), XDDSH(JP)
600 FORMAT(1X, I3, 3(1X, E12.5)//)
590 CONTINUE
C
C CHECK TO SEE WHETHER PLOTS ARE WANTED
      C1=0
      PRINT *, 'ENTER 1 TO PLOT DATA'
      ACCEPT 200, C1
      IF(C1 .EQ. 1) THEN
C CALL PLOT PROGRAM
C CHECK TO SEE WHETHER TO PLOT DISPLACEMENT OR VELOCITY VECTORS
603 TYPE 605
605 FORMAT ('ENTER 1 TO PLOT DISPLACEMENT VECTOR'/
1' ENTER 2 TO PLOT VELOCITY VECTOR'/
1' ENTER 3 TO PLOT ACCELERATION VECTOR'/)
      C1 = 0
      ACCEPT 200, C1
      IF(C1 .NE. 1 .AND. C1 .NE. 2 .AND. C1 .NE. 3) THEN
        PRINT *, 'PLEASE ENTER 1 OR 2 OR 3'
        GO TO 603
      ELSE
        CONTINUE
      ENDIF
      IF(C1 .EQ. 1) CALL PEST (TT, XBARM, ZH, IMAX, NAME)
      IF(C1 .EQ. 2) CALL PEST (TT, XDARM, ZDH, IMAX, NAME)
      IF(C1 .EQ. 3) CALL PEST (TT, ZDDH, XDDSH, IMAX, NAME)
C END OF PLOT ROUTINE
      ELSE
        CONTINUE
      ENDIF
C
      PRINT 610, NAME
      WRITE(6, 610) NAME
610 FORMAT(1X, 'END OF JOB FOR PROGRAM ', 430)
C
C CHECK FOR ANOTHER RUN
      TYPE 620
      NR = 0
620 FORMAT ('ENTER 1 TO MAKE ANOTHER RUN ')
      ACCEPT 200, NR

```

```

      IF (NR .EQ. 1) THEN
C REINITIALIZE NAMES TO ORIGINAL VALUES
      XBAR = XBV
      XDFAR = XDEV
      XDDBAR = XDDBV
      SIG = SIGV
      RMEAN = RMNV
      Z1 = Z1V
      Z01 = Z01V
      ZDD = ZDDV
      B = BV
      G = GV
      H = HV
      K = KV
      T = TV
      TM = TMV
      DELT = DELV
      IMAX = IMAXV
      GO TO 5
    ELSE
      CONTINUE
    ENDIF
C
    STOP
  END

```

# SUBROUTINE PEST

```

SUBROUTINE PEST (TT,XD1,XD2,IMAX,NAME)
C THIS SUBROUTINE PLOTS TIME VERSES TRUE POSITION
CHARACTER *80 NAME
CALL INITT(120)
CALL BINITT
CALL NPTS (IMAX)
CALL CHECK (TT,XD1)
CALL DSPLAY (TT,XD1)
CALL CPLOT (TT,XD2)
CALL LABLIT (80,NAME,312,704,1)
CALL FINITT (0,700)
RETURN
END

```

# SUBROUTINE BETA

```

SUBROUTINE BETA (A)
C THIS PROGRAM CALCULATES BETA
REAL LAM
10 PRINT *, (' PLEASE ENTER TIME CONSTANT ')
READ (5,60,ERR = 10) TC
LAM = - 1./TC
PRINT 40, LAM
40 FORMAT(1X,'THE VALUE OF LAMBDA IS ',F5.2)
50 PRINT *, (' PLEASE ENTER DELT ')
READ (5,60,ERR = 50) DELT
60 FORMAT(1X,F5.2)
PRINT 60, DELT
80 FORMAT(1X,'THE VALUE OF DELT IS ',F5.2)
E = 2.718281828
X = LAM * DELT
PRINT 90, X
90 FORMAT(1X,'LAMBDA * DELT = ',E16.9)
B = E ** X
RETURN
END

```

# SUBROUTINE GAUSS

## SUBROUTINE GAUSS

### PURPOSE

COMPUTES A NORMALLY DISTRIBUTED RANDOM NUMBER WITH A GIVEN MEAN AND STANDARD DEVIATION

### USAGE

CALL GAUSS(IX,S,AM,V)

### DESCRIPTION OF PARAMETERS

IX -IX MUST CONTAIN AN ODD INTEGER NUMBER LESS THAN 32768 ON THE FIRST ENTRY TO GAUSS. THEREAFTER IT WILL CONTAIN A UNIFORMLY DISTRIBUTED INTEGER RANDOM NUMBER GENERATED BY THE SUBROUTINE FOR USE ON THE NEXT ENTRY TO THE SUBROUTINE.  
S -THE DESIRED STANDARD DEVIATION OF THE NORMAL DISTRIBUTION.  
AM -THE DESIRED MEAN OF THE NORMAL DISTRIBUTION  
V -THE VALUE OF THE COMPUTED NORMAL RANDOM VARIABLE

### REMARKS

THIS SUBROUTINE USES RANDU WHICH IS MACHINE SPECIFIC

### SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED

RANDU

### METHOD

USES 12 UNIFORM RANDOM NUMBERS TO COMPUTE NORMAL RANDOM NUMBERS BY CENTRAL LIMIT THEOREM. THE RESULT IS THEN ADJUSTED TO MATCH THE GIVEN MEAN AND STANDARD DEVIATION. THE UNIFORM RANDOM NUMBERS COMPUTED WITHIN THE SUBROUTINE ARE FOUND BY THE POWER RESIDUE METHOD.

.....

SUBROUTINE GAUSS(IX,S,AM,V)

A=0.0

DO 50 I=1,12

CALL RANDU(IX,IY,Y)

IX=IY

50 A=A+Y

V=(A-6.0)\*S+AM

RETURN

END

# SUBROUTINE GHK

```

C THIS SUBROUTINE COMPUTES THE VALUE OF G, H, AND K FROM BETA
C
      SUBROUTINE GHK (G, H, K, Y)
      REAL K, KV
      INTEGER C1
C
C THIS BLOCK DETERMINES IF BETA WILL BE ENTERED FROM THE KEYBOARD
C OR COMPUTED VIA A CALL TO SUBROUTINE BETA.
C
20      PRINT *, ' ENTER 1 IF YOU WANT TO ENTER THE VALUE OF BETA FR
1 THE KEYBOARD'
      NB = 0
      C1 = 0
      READ (5,40,ERR = 20) NB
40      FORMAT (I1)
      IF ( NB .NE. 1) THEN
          CALL BETA (B)
      ELSE
60          PRINT *, ' PLEASE ENTER THE VALUE OF BETA'
          READ (5,80,ERR = 60) B
80          FORMAT (E16.9)
      ENDIF
C
C COMPUTE THE VALUE OF G, H, AND K. RETURN VALUE IN Y
C
      Y = B
      G = 1. - Y **3
      H = 3./2. * ( ( 1. - Y**2) * (1.-Y) )
      K = 1./2. * ( (1.-Y)**3)
90      PRINT 100, Y
100     FORMAT (15X, ' THE VALUE OF BETA IS ',E16.9/)
      WRITE (6,100) Y
105     PRINT 110, G, H, K
110     FORMAT (' G IS ',E12.5,/' H IS ',E12.5,/
1      ' K IS ',E12.5//)
      PRINT *, ' ENTER 1 TO CHANGE VALUE OF BETA'
      ACCEPT 140, C1
      IF (C1 .EQ. 1) GO TO 20
140     FORMAT (I1)
      RETURN
      END

```

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